

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE FOR GAS WELL

Form C-122
Revised 9-1-65

well file

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 9-5-73		SEP 18 1973	
Company Hillen Production Co.				Connection None					
Pool <i>Wildcat Strawn</i> Undesignated Winchester Morrow				Formation Strawn		Unit O. G. C.		ARTESIA OFFICE JCW State	
Completion Date 6-24-72		Total Depth 11257		Plug Back TD 11125		Elevation Casing Head 3290			
Csg. Size 5.5	Wt. 17.20	d	Set At 11257	Perforations: From 10078 To 10099		Well No. 1			
Tbg. Size 2 7/8"	Wt.	d	Set At 10994	Perforations: From To		Unit C		Sec. 2	Twp. 20
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual				Packer Set At 10990		County Eddy			
Producing Thru Csg		Reservoir Temp. °F 175 @ 10089		Mean Annual Temp. °F 74		Baro. Press. - P _a 13.2		State New Mexico	
L	H	Gg	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run 3	Taps FLG.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	3	x	0.625	185	23.0	66	2382	67			1 hr.
2.	3	x	0.625	290	35.5	72	2215	71			1 hr.
3.	3	x	0.625	430	52.5	73	2045	75			1 hr.
4.	3	x	0.625	460	87.0	71	1917	79			1 hr.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	1.850	67.52	198.2	.9943	1.195	1.023	152
2.	1.850	103.75	303.2	.9887	1.195	1.033	234
3.	1.850	152.54	443.2	.9877	1.195	1.052	350
4.	1.850	202.90	473.2	.9896	1.195	1.056	469

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	2.209 Mcf/bbl.
1.	.30	526	1.34	.955	A.P.I. Gravity of Liquid Hydrocarbons	55.1 Deg.
2.	.45	532	1.36	.937	Specific Gravity Separator Gas	.700
3.	.66	533	1.36	.904	Specific Gravity Flowing Fluid	X X X X X
4.	.71	531	1.35	.896	Critical Pressure	668 P.S.I.A.
5.					Critical Temperature	392 R

P _c 2858.2	P _w 8169.3				
NO.	P _c ²	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.838$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.838$
1			5737.0		
2			4964.9		
3			4236.3		
4			3725.8		
5					

Absolute Open Flow	862 Mcfd @ 15.025	Angle of Slope θ	45	Slope, n	1.000
Remarks:					
Approved By Commission:					
Conducted By:		Calculated By:		Checked By:	
J. C. Roberts		J. C. Roberts			