

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

R 100 7 60

Type Test ☐ Initial ☐ Annual ☒ Special					Test Date 11-29-73		DEC 1 1973	
Company Hillin Production Co.				Connection El Paso				
Pool <u>R4734</u> 3-1-74 Winchester				Formation Strawn				Unit <u>ARTESIA, LA BIDE</u>
Completion Date 6-24		Total Depth 11257		Plug Back TD 11125		Elevation 3290 C.H.		Farm or Lease Name JCW - State <u>Com</u>
Csg. Size 5 1/2	Wt. 17.20	Id	Set At 11257	Perforations: From 10078 To 10099		Well No. 1-Com:		
Thq. Size	Wt.	Id	Set At	Perforations: From To		Unit C	Sec. 2	Twp. 20
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual				Packer Set At 10990		County Eddy		
Producing Thru Casing		Reservoir Temp. °F 175 @ 10089		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico
L	H	Gg .688	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run 4.026	Taps Flg.

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI									2515	60	
1.	4.026		1.25	9.70	1.6	70			2227	80	1 hr.
2.			"	9.75	3.2	65			1883	83	1 hr.
3.			"	9.75	4.4	65			1553	79	1 hr.
4.			"	9.80	6.3	66			1310	74	1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{\frac{h_w P_m}{L - 10}}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	7.469		15.52	(3.162)	.9905	1.206	437.8
2.	"		31.20		.9952	"	884.4
3.	"		42.90		.9952	"	1216.0
4.	"		61.74		.9943	"	1748.5
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio <u>12.948</u> Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons <u>55.1</u> Deg.
2.					Specific Gravity Separator Gas <u>XXXXXXX</u>
3.					Specific Gravity Flowing Fluid <u>XXXXX</u>
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c <u>2528.2</u>	P _c ² <u>6392</u>	
NO.	P _t ²	P _w ²
1	2240.2	5018
2	1896.2	3596
3	1566.2	2453
4	1323.2	1751
5		

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.623$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.576$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1916$

Absolute Open Flow <u>1916</u> Mcfd @ 15.025	Angle of Slope <u>44.1°</u>	Slope, n <u>.971</u>
Remarks:		
Approved By Commission:	Conducted By: C. Allen Dorsey	Calculated By: C. Allen Dorsey
		Checked By: