

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

CORRECTED COPY - JULY 16 1976

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Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 7/6/76		JUL 20 1976	
Company The Superior Oil Company			Connection Llano		
Pool Wildcat			Formation Morrow		Unit O. G. C. ARTESIA, OFFICE
Completion Date 6/6/73		Total Depth 11476		Plug Back TD 11370	
Elevation 3293 GR		Farm or Lease Name State "Q" Com			
Csg. Size 7"-5"	Wt. 18#	Id. 	Set At 	Perforations: From 11086 To 11244	
Thq. Size 2-7/8"	Wt. 6.5	Id. 2.441	Set At 10999	Perforations: Open Ended	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single			Packer Set At 10,998		County Eddy
Producing Thru Tubing		Reservoir Temp. °F 188 @ 11260		Mean Annual Temp. °F 60	
Baro. Press. - P _a 13.2		State New Mexico			
L 10999	H 10999	G _g .602	% CO ₂ 1.35	% N ₂ .28	% H ₂ S
Prover 		Meter Run 4"		Taps Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	4.026						2302		Pkr.		43
1.			1.5	740	9	79	1342	60			2-1/4
2.			1.5	755	12	74	1140	60			2
3.			1.5	760	14	75	990	60			1-1/4
4.			1.5	765	16	74	882	60			3/4
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	10.84	82.33	753.2	.9822	1.289	1.059	1196
2	10.84	96.01	768.2	.9868	1.289	1.059	1402
3	10.84	104.0	773.2	.9859	1.289	1.060	1518
4	10.84	111.6	778.2	.9868	1.289	1.061	1633
5							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas .602 XXXXXXXXXX
3.					Specific Gravity Flowing Fluid XXXXXX
4.					Critical Pressure 676 P.S.I.A. P.S.I.A.
5.					Critical Temperature 357 R R

P _c 2315	P _c ² 5359		
NO.	P _f ²	P _w ²	P _c ² - P _w ²
1		1362	1855
2		1163	1353
3		1017	1034
4		913	834
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.184309$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.184309$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1934$$

Absolute Open Flow 1934 Mcfd @ 15.025	Angle of Slope θ 45°	Slope, n 1
Remarks: _____		
Approved By Commission:	Conducted By: Ernie Hanson	Calculated By: P.R. Blancett
Checked By:		