

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

0 C-122
Form C-122
Revised 9-1-68

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AUG 15 1973

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 8-1-73			
Company Coquina Oil Corp.				Connection None					
Pool Burton Flat				Formation Morrow				Unit AUG 15 1973	
Completion Date		Total Depth 11,614		Plug Back TD 11,580		Elevation 3275 KB		Farm or Lease Name C. C. Yata	
Csg. Size 7	Wt. 23	d 11,614	Set At 11,614	Perforations: From 11,454 To 11,513		Well No. 1			
Tub. Size 2 7/8	Wt. 6.8	d 11,512	Set At 11,512	Perforations: From To		Unit 10		Sec. Twp. Rge. 21S 27E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G. G. Dual						Packer Set At 11,403		County Eddy	
Producing Thru Morrow		Reservoir Temp. °F 189 @ 11,512		Mean Annual Temp. °F 13.2		Baro. Press. - P _a		State New Mexico	
L 11,512	H 11,512	Ga 575	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run 3"	Taps Flg.	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	3	x	1.750	538	5"	100	3691	84			72hr sig
2.	3	x	1.750	530	17"	100	3582	82			2'
3.	3	x	2.000	550	51"	44	3108	80			2'
4.	3	x	2.000	560	87"	33	2841	77			2'
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	15.61	52.50	551.2	.9636	1.319	1.031	1,074
2	15.61	96.10	543.2	.9636	1.314	1.031	1,966
3	21.32	169.48	563.2	1.016	1.319	1.049	5,079
4	21.32	223.31	573.2	1.027	1.319	1.055	6,804
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.82	560	1.62	.940	Dry	None	.575	X X X X X X X X	672	346
2	.81	560	1.62	.940						
3	.84	504	1.46	.908						
4	.85	493	1.42	.899						
5										

P _c 3777.2 P _w 14,267.2				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.989$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.590$	
NO.	P _r	P _w	P _r ²	P _w ²	P _r ² - P _w ²		
1	13721.1	3713.7	13791.6	475.6			
2	12925.5	3615.9	13074.7	1192.5			
3	9741.9	3298.9	10882.7	3384.5			
4	8146.5	3081.3	9494.4	4772.8			
5							

ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 17.621$

checked 8-11-73

Absolute Open Flow 17,621 Mcfd @ 15.025		Angle of Slope 49	Slope, n .869
Remarks: B. H. B. Set at 11,375 180° BHT 1.76 BBLS. H ₂ O			

Approved By Commission:	Conducted By: Reggie Reston	Calculated By: Reggie Reston	Checked By:
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