

NEW MEXICO CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date JUL 19 1973	
Company Atlantic Richfield Company			Connection Not Connected		O. C. C. ARTESIA, OFFICE	
Pool Undesignated			Formation Cisco		Unit	
Completion Date 7-1-73		Total Depth 11150		Plug Back TD 9586	Elevation 3185 DF	Farm or Lease Name State B0 COM
Csq. Size 4-1/2"	Wt. 11.6	d 4.000	Set At 9610	Perforations: From 9280 To 9455		Well No. 1
Tbg. Size 2 - 3/8"	Wt. 4.7	d 1.995	Set At 9217	Perforations: From Open To Ended		Unit Sec. Twp. Rge. G 15 21S 26E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 9217		County Eddy
Producing Thru Tbg. 9217		Reservoir Temp. °F 140° 9290		Mean Annual Temp. °F 60		Baro. Press. -- P _a 13.2
L 9217		H 9217	G _g 0.5984	% CO ₂ Trace	% N ₂ 0.04	% H ₂ S 0
				Prover	Meter Run 4"	Taps Flg.

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2836				72 Hr. S.I.
1.	4 x 1.500			200	5	83	2750	75	Pkr.		1 Hr.
2.	4 x 1.500			215	11	83	2679	75			1 Hr.
3.	4 x 1.500			305	12	85	2590	75			1 Hr.
4.	4 x 1.500			400	13	85	2474	76			1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	10.84	32.65	213.2	0.9786	1.293	1.016	455
2	10.84	50.10	228.2	0.9786	1.293	1.017	699
3	10.84	61.79	318.2	0.9768	1.293	1.023	865
4	10.84	73.29	413.2	0.9768	1.293	1.030	1034
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.32	543	1.53	0.969	A.P.I. Gravity of Liquid Hydrocarbons	56.3 Deg.
2.	0.34	543	1.53	0.967	Specific Gravity Separator Gas	0.5984 XXXXXXXX
3.	0.47	545	1.54	0.956	Specific Gravity Flowing Fluid	0.6025 XXXXXX
4.	0.61	545	1.54	0.943	Critical Pressure	672 P.S.I.A.
5.					Critical Temperature	354 °R

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 9.460$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.083$
1	7635.3		7641.9	476.0		
2	7247.9		7259.8	858.1		
3	6776.7		6797.5	1320.4		
4	6186.2		6214.1	1903.8		
5						

Absolute Open Flow 2155		Mcf @ 15.025	Angle of Slope @ 30° - 4'	Slope, n 0.501
Remarks:				
Approved By Commission:	Conducted By: Jerry Guy	Calculated By: L. C. Hudry	Checked By: L. C. Hudry	

Witness K. Hooten, Southern Union