

MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

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FILE

Type Test: ☐ Initial ☐ Annual ☒ Special		Test Date 7-31-85		O. C. D. ARTESIA, OFFICE	
Company Amoco Production Company			Connection Llano		
Pool Golden Lane Strawn			Formation Strawn		Unit
Completion Date 7-31-85		Total Depth 12,612'	Plug Back TD 11,624'	Elevation 3337	Farm or Lease Name Fed. "G" Gas Com
Csg. Size 5.5	Wt. 4.7	d 4.778	Set At 12,612	Perforations: From 10,973 To 11,042	Well No. 1
Tqg. Size 2.375	Wt. 4.7	d 1.995	Set At 10,853	Perforations: From -- To --	Unit Sec. Twp. Rge. J 21 20S 30E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10,750	County Eddy
Producing Thru Tubing		Reservoir Temp. °F 180 @ 11,008	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2	State New Mexico
L 11,008	H 11,008	G _g 0.670	% CO ₂ 0.0	% N ₂ 0.0	% H ₂ S 0.0
				Prover 3.0	Meter Run Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI										
1.	3.0 x 1.500			610	10	75	3178	81	190	81
2.	3.0 x 1.500			618	14	74	2910	72	-	-
3.	3.0 x 1.500			618	28	71	2780	70	-	-
4.	3.0 x 1.500			620	79	62	2590	73	-	-
5.							2500	72	-	-

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	11.17	78.94	623.2	0.9859	1.2217	1.0630	1129
2	11.17	94.00	631.2	0.9868	1.2217	1.0643	1347
3	11.17	132.94	631.2	0.9896	1.2217	1.0657	1913
4	11.17	223.66	633.2	0.9981	1.2217	1.0712	3262
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.93	535	1.41	.885	37.1	76.9	.670	XXXXXX	669	380
2.	.94	534	1.40	.883						
3.	.94	531	1.40	.880						
4.	.95	522	1.37	.872						
5.										

P _c 3158.3	P _c ² 9975	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.1230$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.2446$
NO. 1	P _w 8545	P _w ² 2912	P _c ² - P _w ² 1497
2	7805	2788	7774
3	6777	2604	6781
4	6316	2558	6544
5			

Absolute Open Flow 4294 Mcfd @ 15.025		Angle of Slope θ 54.5	Slope, n 0.71
Remarks: Point #4 erroneous, first 3 points used for calculation			
Approved By Commission:		Conducted By:	Calculated By: Barbara Wagner
			Checked By: Mike Madere