

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 11-23-73		DEC 20 1973	
Company David Fasken			Connection None		
Pool Wildcat			Formation Strawn		
Completion Date 11-23-73		Total Depth 11240		Plug Back TD 10945	
Elevation 3204 KB		Farm or Lease Name El Paso "3" Federal			
Csq. Size 5 1/2	Wt. 20 & 23	d 4.67	Set At 10997	Perforations: From 9847 To 9922	
Tbg. Size 2 7/8	Wt. 6.5	d 2.441	Set At 9647	Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single (Plug @ 10650')				Packer Set At 9647	
Producing Thru Tubing		Reservoir Temp. °F 170 @ 9600		Mean Annual Temp. °F 70	
Baro. Press. - P _a 13.2		State New Mexico			
L 9885	H 9885	G _g 0.780	% CO ₂	% N ₂	% H ₂ S
Prover		Meter Run X		Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3337		Pkr.		
1.	6"	X	2"	615	44.5	66	3112	70	"		60 min.
2.	6"	X	2"	610	21	68	3112	70	"		60 min.
3.	6"	X	2"	580	7	82	3147	70	"		60 min.
4.	6"	X	1"	600	48	84	3165	70	"		60 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor F _{pv}	Rate of Flow Q, Mcfd
1	19.160	167.20	628.2	0.9943	1.132	1.101	3969.9
2	19.160	114.40	623.2	0.9924	1.132	1.101	2711.1
3	19.160	64.44	593.2	0.9795	1.132	1.085	1485.4
4	4.726	171.56	613.2	0.9777	1.132	1.090	978.1
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	47.176	Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons	59	Deg.
2.	Used Simplified				Specific Gravity Separator Gas	0.780	XXXXXXXXXX
3.	Supercompressibility Tables				Specific Gravity Flowing Fluid	XXXXXX	
4.					Critical Pressure	666	P.S.I.A.
5.					Critical Temperature	418	R

P _f 4297.2 P _{f2} 18466			
NO.	P _i ²	P _s	P _s ² P _{f2} ² - P _s ²
1		4058.2	16469 1998
2		4066.2	16534 1932
3		4102.2	16828 1638
4		4126.2	17026 1440
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{P_c^2}{P_c^2 - P_w^2}$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{P_c^2}{P_c^2 - P_w^2}$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{P_c^2}{P_c^2 - P_w^2}$

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Absolute Open Flow	37,000	Mcf/d @ 15.025	Angle of Slope	450	Slope, n	1.000
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Remarks: Bottom hole pressures measured with Amerada RPG-3 gauge.
Decreasing sequence used to assure liquid removal.

Approved By Commission:	Conducted By: Tefteller, Inc.	Calculated By: F. Tefteller	Checked By:
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