

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

*Copy to SF
C-122*

Type Test <input checked="" type="checkbox"/> Initial <input type="checkbox"/> Annual <input type="checkbox"/> Special				Test Date 3-20-74		RECEIVED	
Company Texas Oil & Gas Company				Connection To Air			
Pool Burton Flat				Formation Morrow		Unit APR 8 1974	
Completion Date		Total Depth 11751		Plug Back TD 11666		Elevation	
Csq. Size 4 1/2		Set At 11751		Perforations: From 11346 To 11451		Well No. 3	
Tbg. Size 2 3/8		Set At 11275		Perforations: From To		Unit Sec. Twp. Rge. E 17 20S 29E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 11,213		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 186 @ 11370'		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2	
L 11370		H 11370		G _g 0.661		% CO ₂ 0.87	
				% N ₂ 0.45		% H ₂ S -0-	
				Prover 2"		Meter Run Taps	
FLOW DATA				TUBING DATA		CASING DATA	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.
NO.						Temp. °F	Press. p.s.i.g.
1.	2" x 1.250"			57.0		40	2295.0
2.	2" x 1.250"			40.0		36	2773.0
3.	2" x 1.250"			21.0		64	3157.0
4.	2" x 1.250"			8.0		64	3377.0
5.							
RATE OF FLOW CALCULATIONS							
NO.	Q Before Correction (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	2594	Not Applicable	Not Applicable	1.0198	.9528	1.000	2521
2.	1980			1.0239	.9528	1.000	1932
3.	1270			.9962	.9528	1.000	1205
4.	700			.9962	.9528	1.000	664
5.							
NO.	P _i	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ TSM Mcf/bbl.		
1.	Not Applicable	- All			A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.		
2.	pressures less than 100 psig				Specific Gravity Separator Gas 0.661 X X X X X X X X		
3.					Specific Gravity Flowing Fluid X X X X X		
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.		
5.					Critical Temperature _____ R _____ R		
$P_i = 4737.2$ $P_w = 2244.1$							
NO.	P _i ²	P _w	P _w ²	P _i ² - P _w ²	(1) $\frac{P_c^2}{P_i^2 - P_w^2} = 1.9887$		(2) $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 1.6833$
1.		3340.2	11157	11284			
2.		3819.2	14586	7855			
3.		4257.2	18124	4317			
4.		4497.2	20225	2216			
5.					AOF = Q $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 4244$		
Absolute Open Flow 4244 Mcfd @ 15.025				Angle of Slope @ 52.8°		Slope, n 0.760	
Remarks: Volumes obtained from meria tables and corrected for temp & Sp Gr							
RECEIVED							
Approved By Commission:		Conducted By: D. Tyson - J. Smith		Calculated By: R. West		Checked By: APR 8 1974	