

JUL 15 1974

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 7-1-74			
Company Monsanto Company		Connection		O.C.C. ARTESIA, OFFICE	
Pool Burton Flat <i>Morrow</i>		Formation Morrow		Unit F	
Completion Date 7-1-74 3-19-74		Total Depth 11,700		Plug Back TD 11,638	
Elevation 3285 DF		Farm or Lease Name Wilderspin			
Cas. Size 7"	Wt. 26#	Set At 11,700	Perforations: From 11,326 To 11,616		Well No. 1-14
Reg. Size 2 3/8	Wt. 4.7	Set At 11,100	Perforations: From To		Unit Sec. Twp. Rge. F 11 21-S 27-E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Triple				Packer Set At 11,100	
Producing Thru Tubing		Reservoir Temp. °F 165 @ 11,700		Mean Annual Temp. °F	
Baro. Press. - P _a		State New Mexico			
L 11471	H 11471	G _g .604	% CO ₂	% N ₂	% H ₂ S
Prover		Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1840	76			
1.	4.0		2.125	780	2.5	85	1365	78			1 Hr
2.	4.0		2.125	780	3.5	85	1175	82			1 Hr
3.	4.0		2.125	780	5.0	86	1042	85			1 Hr
4.	4.0		2.125	780	6.5	87	945	87			1 Hr
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	22.60	44.53	793.2	.9768	1.2867	1.061	1342
2	22.60	52.69	793.2	.9768	1.2867	1.061	1588
3	22.60	62.97	793.2	.9759	1.2867	1.060	1894
4	22.60	71.80	793.2	.9750	1.2867	1.060	2158
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	None Produced	Mcft/bbl.
1	1.20	545	1.52	.888	A.P.I. Gravity of Liquid Hydrocarbons		Deq.
2	1.20	545	1.52	.888	Specific Gravity Separator Gas	.604	X X X X X X X X
3	1.20	546	1.53	.890	Specific Gravity Flowing Fluid	X X X X X	
4	1.20	547	1.53	.890	Critical Pressure	671	P.S.I.A. 671 P.S.I.A.
5					Critical Temperature	358	R 358 R

P _c 1853.2	P _c ² 3434		
NO.	P _t ²	P _w	P _w ²
1		1401.6	1964
2		1206.9	1457
3		1112.2	1237
4		1040.0	1082
5			

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{3434}{1470} \quad (2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.13513$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2865$$

Absolute Open Flow 2865 Mcfd @ 15.025		Angle of Slope @ 64° 3'		Slope, n .894	
Remarks: Well Shut-In 47.3 Hours Prior to Starting This Test/					
Approved By Commission:		Conducted By: W T Hagler		Calculated By: H L Hagler	
		WEST TEXAS CONSULTING SERVICE, INC.		Checked By:	