

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 1/8/91		MAR 29 1991	
Company Oxy USA, Inc.		Connection Vented		O. C. D. ADDITIONAL CHARGE	
Pool Burton Flat		Formation Morrow		Unit	
Completion Date 1/8/91		Total Depth 12165		Plug Back TD 11910	
		Elevation 3148.0 G.L.		Farm or Lease Name Simpson A	
Csg. Size 5 1/2		Set At 12165		Performances: From 11624 To 11809	
Tbg. Size 2 3/8		Set At 11556		Performances: From open To end	
Type Well - Single - Broadhead - G.C. or G.O. Multiple Single		Packer Set At 11556		Well No. 2-Z	
Producing Thru Tbg.		Reservoir Temp. °F 191 @ 11716		Mean Annual Temp. °F 60	
		Baro. Press. - P _a 13.2		State NM	
L *11716		H *11716		Cg .598	
		% CO ₂ 1.07		% N ₂ 0.48	
		% H ₂ S		Prover 3.826	
				Meter Run flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. In. Hg	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2242		Pkr.		24 Hrs.
1.	4 x	1.250		470	3.00	75	1917		Pkr.		1 Hr.
2.	4 x	1.250		480	8.00	94	1858		Pkr.		1 Hr.
3.	4 x	1.250		490	28.00	72	1558		Pkr.		1 Hr.
4.	4 x	1.250		490	41.00	58	1410		Pkr.		1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_{LP} P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	7.483	38.07	483.2	.9859	1.293	1.038	377
2	7.483	62.81	493.2	.9688	1.293	1.031	607
3	7.483	118.70	503.2	.9887	1.293	1.039	1,180
4	7.483	143.64	503.2	1.002	1.293	1.044	1,454
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcft/bbl.
1.	.71	535	1.51	.929	A.P.I. Gravity of Liquid Hydrocarbons	Dry	Deq.
2.	.72	554	1.56	.940	Specific Gravity Separator Gas	.598	XXXXXXXXXX
3.	.74	532	1.50	.926	Specific Gravity Flowing Fluid	XXXXXX	
4.	.74	518	1.46	.917	Critical Pressure	**676	P.S.I.A.
5.					Critical Temperature	**353	R

NO.	P _r ²	P _w	P _r ²	P _r ² - P _w ²
1		1935.4	3745.8	1288.4
2		1883.0	3545.7	1488.5
3		1604.1	2573.1	2461.1
4		1499.1	2247.3	2786.9
5				

(1) $\frac{P_c^2}{P_r^2 - P_w^2} = 1.806$

AOF = Q $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 2.626$

(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.806$

Post FD-2
4-12-91
comp + BK

Absolute Open Flow	2,626	Mcfd @ 15.025	Angle of Slope °	45	Slope, n	1.000
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Remarks: * = BHP instrument set @ this depth
 ** = Corrected to 1.07% CO₂ (No fluid produced)
 *** = BHP from shut-in corrected to surface pressure (psia)

Approved By Division	Conducted By: John West Engineering	Calculated By: BM	Checked By: BM
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