

Copy 6-51
Form C-122
Revised 9-1-65

MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED

Type Test ☒ Initial ☐ Annual 60 Day ☐ Special				Test Date 5-1-75		MAY 26 1975	
Company Inexco Oil Company				Connection Southern Union Gas Co.		O. C. C. ARTESIA, OFFICE	
Pool Catchlaw Draw 7, 1960				Formation Morrow		Unit	
Completion Date Sept. 9, 1974		Total Depth 11000		Plug Back TD 10968		Elevation 3345GL 3360 KB	
Csg. Size 5 1/2		Wt. 15		Set At 10999		Perforations: From 10746 To 10887	
Tubg. Size 2 3/8		Wt. 4.7		Set At 10650		Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10650		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 182 @ 10600		Mean Annual Temp. °F 70		Baro. Press. - P _a 13.2	
L 10817		H 10817		G _g 0.623		% CO ₂ % N ₂ % H ₂ S Prover	
						Meter Run X	
						Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. L-10	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI	72 hrs.			634.8		70	3020		Pkr		
1.	4"	X	3/4"	642.9	2.60	77	2957	70	"		60 min.
2.	4"	X	3/4"	642.9	4.20	81	2913	70	"		60 min.
3.	4"	X	3/4"	642.9	6.50	80	2862	70	"		75 min.
4.	4"	X	3/4"	642.9	9.35	80	2735	70	"		180 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	2.661	20.93	648.0	0.9840	1.267	1.056	231.9
2.	2.661	34.02	656.1	0.9804	1.267	1.055	375.1
3.	2.661	48.60	656.1	0.9813	1.267	1.055	536.4
4.	2.661	75.74	656.1	0.9813	1.267	1.055	835.9
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry Gas	Mcf/bbl.
1.	0.97	537	1.47	0.897	A.P.I. Gravity of Liquid Hydrocarbons	Dry Gas	Deq.
2.	0.98	541	1.48	0.899	Specific Gravity Separator Gas	0.623	X X X X X X X X
3.	0.98	540	1.48	0.899	Specific Gravity Flowing Fluid	X X X X X	
4.	0.98	540	1.48	0.899	Critical Pressure	671	P.S.I.A.
5.					Critical Temperature	366	R

P _f 3880.2 P _f ² 15056				
NO.	P _i ²	P _s ²	P _s ²	P _f ² - P _s ²
1		3801.2	14449	607
2		3748.2	14049	1007
3		3680.2	13544	1512
4		3522.2	12406	2650
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{P_c^2}{P_c^2 - P_w^2}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{P_c^2}{P_c^2 - P_w^2}$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{P_c^2}{P_c^2 - P_w^2}$

Absolute Open Flow	4100	Mcf/d @ 15.025	Angle of Slope @	47° 57'	Slope, n	0.902
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Remarks: BHP measured with Amerada RPG-3 gauge
Serial No. 31203N 0-6000 psi

Approved By Commission:	Conducted By: Tefteller, Inc.	Calculated By: F. Tefteller	Checked By: <i>[Signature]</i>
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