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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

JAN 12 '95

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator OXY U.S.A.				Lease or Unit Name GOVERNMENT Z			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 12-20-94		Well No. 1	
Completion Date 12-17-94		Total Depth 11485		Plug Back TD 11367		Elevation	
Csg. Size 5 1/2		Wt. 15.5		d 4.950		Set At 11485'	
Tbg. Size 2-7/8		Wt. 6.5		d 2.441		Set At 11323'	
Perforations: From: 11342 To: 11348				County Eddy			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple single				Packer Set At 11323		Formation MORROW	
Producing Thru Tbg.		Reservoir Temp. °F 187 @ 11200		Mean Annual Temp. °F 60°		Baro. Press - P _a 1.32	
*11200		H ₂ *11200		Gg.597		% CO ₂ .90	
				% N ₂ .20		% H ₂ S	
				Prover		Meter Run 6.065	
						Taps PLG.	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3260				
1.	6.065	X	2.750	600	6	60	3130		PKR.		1 hr.
2.	6.065	X	2.750	615	19	68	3000				1 hr.
3.	6.065	X	2.750	630	40	63	2750				1 hr.
4.	6.065	X	2.750	630	52	58	2600				1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	36.99	60.66	613.2	1.000	1.294	1.062	3084
2.	36.99	109.25	628.2	.9924	1.294	1.056	5480
3.	36.99	160.40	643.2	.9971	1.294	1.066	8161
4.	36.99	182.88	643.2	1.002	1.294	1.066	9350
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	122.954	Mcf/bbl.
1.	.91	520	1.43	.886	A.P. I. Gravity of Liquid Hydrocarbons	49.4 @ 60°	Deg.
2.	.94	528	1.45	.896	Specific Gravity Separator Gas	.597	XXXXXXXXXX
3.	.96	523	1.43	.880	Specific Gravity Flowing Fluid	.784 XXXXX	GMIX=.623
4.	.96	518	1.42	.880	Critical Pressure	672	P.S.I.A. 671 P.S.I.A.
5.					Critical Temperature	354	R 365 R

P _c 3331.0	P _c ² 11095.56						
NO.	P _c ²	P _w	P _w ²	P _c ² - P _w ²	1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.98480$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.75663$	
1.	3243.6	10520.94	574.62				
2.	3161.5	9995.08	1100.48				
3.	3033.3	9200.91	1894.65				
4.	2978.2	8869.68	2225.88				
5.							

Absolute Open Flow	35,125	Mcf @ 15.025	Angle of Slope θ	50.5°	Slope, n	.82391
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Remarks: * BOTTOM HOLE PRESSURE INSTS. HUNG @ THIS DEPTH.

CALCULATED USING KNOWN BOTTOM HOLE PRESSURES-(8 BBLS 49.4 GRAVITY COND. MADE DURING TEST)

Approved By Division

Conducted By
PRO WELL TESTER

Calculated By
KS

Checked By
BM