

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 01/30/75		FEB 6 1975	
Company Atlantic Richfield Company				Connection None		O. C. C. ARTESIA, OFFICE	
Pool Avalon Morrow Gas				Formation Morrow		Unit	
Completion Date 01/20/75		Total Depth 11,100		Plug Back TD 10,996		Elevation 3280.6 G.L.	
Casing Size 5.5		Wt. 17.0		d 4.892		Set At 11096	
Tbg. Size 2		Wt. 4.7		d 1.995		Set At 10779	
Performations: From 10867 To 10916				Well No. 1			
Performations: From Open Ended				Unit O		Sec. Twp. Rge. 9 21-S 26-E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10748		County Eddy	
Producing Thru Tbg		Reservoir Temp. °F # 186		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
L 10779		H 10779		G _a 0.5898		State New Mexico	
% CO ₂ 0.609		% N ₂ 1.191		% H ₂ S -0-		Prover ---	
Meter Run 4"		Taps Flg.					

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. in. H ₂ O	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3483	55	Pkr		116 hr.
1.	4 x 1.000			615	79.0	77	2412	59			1 hr.
2.	4 x 1.000			710	41.0	78	2700	59			1 hr.
3.	4 x 1.000			710	16.0	68	3048	59			1 hr.
4.	4 x 1.000			630	8.0	92	3291	57			0.8 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1	4.753	222.77	628.2	.9840	1.302	1.043	1415.2
2	4.753	172.20	723.2	.9831	1.302	1.049	1099.3
3	4.753	107.57	723.2	.9924	1.302	1.053	695.8
4	4.753	71.73	643.2	.9706	1.302	1.039	447.7
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.93	537	1.55	.919	-0-	-0-	0.5898	XXXXXXX	672.6	345.6
2	1.08	538	1.56	.908				XXXXX		
3	1.08	528	1.53	.901						
4	.96	552	1.60	.926						
5										

NO.	P _i ²	P _w	P _w ²	P _i ² - P _w ²
1	5881.6	2457.1	6037.3	6186.1
2	7361.5	2745.9	7539.8	4683.6
3	9370.9	3091.8	9559.3	2664.2
4	10917.7	3335.8	11127.8	1095.6
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.976$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2502$$

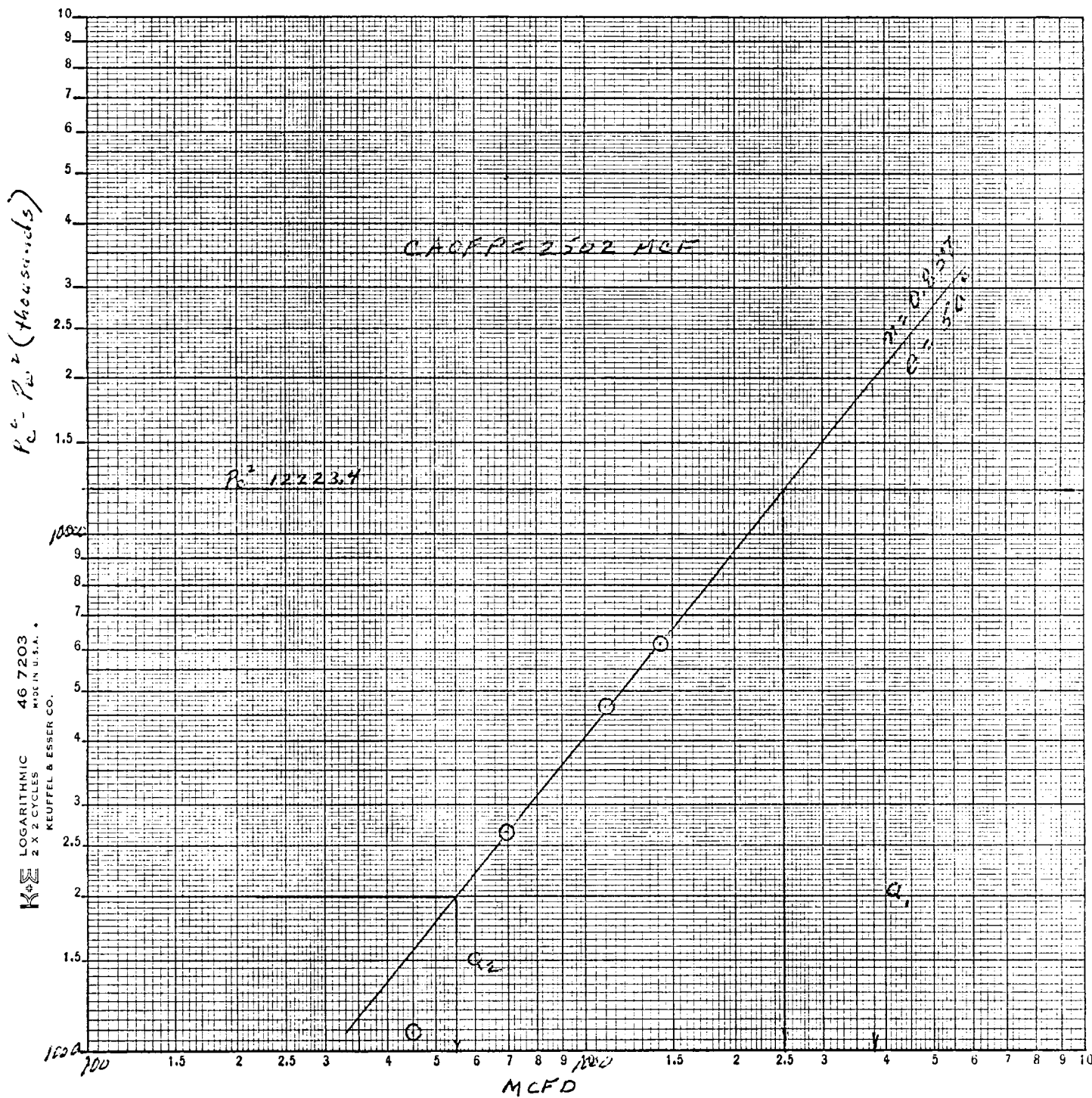
$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.768$$

Absolute Open Flow	2502	Mcfd @ 15.025	Angle of Slope θ	50	Slope, n	0.837
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Remarks: Calculated by computer

Approved By Commission:	Conducted By: J. Coleman	Calculated By: J. Coleman	Checked By: P. Huff
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ATLANTIC RICHFIELD COMPANY
 BQ-2 Federal Com #1
 Unit O, S-0, T-21-S, R-26-E
 Eddy County, N.M.
 01/30/75



AP 20000
 AP 2000

3750 MCF $\log Q_1 = 3.577492$
 550 MCF $\log Q_2 = 2.740363$

$$n = 0.837129 = 0.837$$

