

**NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

RECEIVED

Copy 631
C-122

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 3-27-75		APR 14 1975	
Company C & K Petroleum, Inc.				Connection None		O. C. C. ARTESIA, OFFICE	
Pool Undesignated				Formation Delaware-Brushy Canyon		Unit	
Completion Date 3-21-75		Total Depth 11,720 feet		Plug Back TD 4,225 feet		Elevation 3,423 KB	
Csg. Size 7"		Wt. 23&26#/ft		Set At 4,252.8		Perforations: From 4,137 To 4,154	
Tbg. Size 2-3/8"		Wt. 4.70		Set At 4,109		Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 4,109		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 98 @ 4,154		Mean Annual Temp. °F 70		Baro. Press. - P _a 13.2	
State New Mexico							
L 4,154	H 4,154	G _g .700	% CO ₂ Nil	% N ₂	% H ₂ S Nil	Prover	Meter Run 4"
						Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI						50	1,700	50	Packer	
1.	4"		1.500	370	61	74	1,420	72		4 hrs.
2.	4"		1.500	360	35	76	1,450	72		1-1/2 hrs.
3.	4"		1.500	360	17	74	1,500	66		2-1/2 hrs.
4.	4"		1.500	350	8	76	1,480	54		11-1/2 hrs.
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	10.84	152.8895	383.2	0.9868	1.195	1.042	2,036
2	10.84	118.2937	373.2	0.9850	1.195	1.042	1,519
3	10.84	79.6517	373.2	0.9868	1.195	1.042	1,061
4	10.84	53.9036	363.2	0.9850	1.195	1.042	717
5							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons 50.5 _____ Deg.
2.					Specific Gravity Separator Gas .700 _____ XXXXXXXXXX
3.					Specific Gravity Flowing Fluid XXXXX _____
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

$P_t = 1,965.2 * P_w^2 = 3,862$				
NO.	P _t	P _w	P _w ²	P _t ² - P _w ²
1		1,753.4	3,075	787
2		1,787.1	3,194	668
3		1,817.4	3,303	559
4		1,831.8	3,355	507
5				

(1) $\frac{P_t^2}{P_t^2 - P_w^2} = \frac{11.9}{11.9 - 11.8} = 11.9$

AOF = Q $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 5,462$

(2) $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 7.617$

Absolute Open Flow	5,462	Mcf @ 15.025	Angle of Slope	45°	Slope, n	1.000
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Remarks: *Bottom Hole Pressure @Bottom Perforations - 4,154'

Approved by Commission	Conducted By: C. Allen Dorsey	Calculated By: C. Allen Dorsey	Checked By: Wm. P. Aycok, P. E.
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