

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED

Form C-122
Revised 1-65

Type Test ☐ Initial ☐ Annual ☐ Special					Test Date 3-19-91				
Company OXY USA, INC					Ventilation VENTED				
Pool BURTON FLAT					Unit MORROW				
Completion Date 3-19-91		Total Depth 11575		Plug Back TD 11540		Elevation 3121 GL		Farm or Lease Name TRACY D.	
Csg. Size 5 1/2	Wt. 17 & 20	d 11575	Set At 11575	Perforations: From 11133 To 11441		Well No. 1			
Thq. Size 2 3/8	Wt. 4.7	d 1.995	Set At 11078	Perforations: From OPEN To END		Unit K	Sec. 33	Twp. 21	Rge. 27
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE					Packer Set At 11080		County EDDY		
Producing Thru TB6		Reservoir Temp. °F 187° 11286		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State NEW MEXICO	
L 1-1286	H 11286	Gg .601	% CO ₂ 2.26	% N ₂ .27	% H ₂ S	Prover	Meter Run 4.026	Taps FLG	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3165		PKR		72 HRS
1.	4 x 1.250			495	10.00	74	2600		PKR		1 HR
2.	4 x 1.250			500	15.00	88	1950		PKR		1 HR
3.	4 x 1.250			500	20.00	76	1712		PKR		1 HR
4.	4 x 1.250			500	40.00	62	1290		PKR		1 HR
5.	4 x 1.250			520	45.00	62	805		PKR		1 HR

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	7.469	71.29	508.2	.9868	1.290	1.039	704
2	7.469	87.74	513.2	.9741	1.290	1.040	856
3	7.469	101.31	513.2	.9850	1.290	1.040	1,000
4	7.469	143.28	513.2	.9981	1.290	1.045	1,440
5	7.469	154.90	533.2	.9981	1.290	1.047	1,560

NO.	R _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio	DRY GAS	Mcf/bbl.
1	.74	534	1.50	.926	A.P.I. Gravity of Liquid Hydrocarbons	DRY	Deq.
2	.75	548	1.54	.925	Specific Gravity Separator Gas	.601	X X X X X X X X
3	.75	536	1.50	.925	Specific Gravity Flowing Fluid	X X X X X	
4	.75	522	1.47	.916	Critical Pressure	*679	P.S.I.A. P.S.I.A.
5	.78	522	1.47	.912	Critical Temperature	*355	R R

*** P_c 3865.4 P_c² 14941.3

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1		2827.4	7994.2	6947.0
2		2499.5	6247.5	8693.8
3		2260.3	5109.0	9832.3
4		1656.1	2742.7	12198.6
5		1256.8	1579.6	13361.7

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.118$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.118$

ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.744$

Part ID-2
5-12-91
comp. Mor

Absolute Open Flow	1.744	Mcf/d @ 15.025	Angle of Slope @	45	Slope, n	1.000
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Remarks: *CORRECTED TO 2.26 % CO₂. WELL MADE 5 BBLS. N₂O DURING TEST. ** BNP INSTRUMENT SET AT THIS DEPTH. *** KNOWN BNP'S CALCULATED BACK TO SURFACE PRESSURES.

Approved By Commission:	Conducted By: JOHN WEST ENGINEERING	Calculated By: B.M.	Checked By: B.M.
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