

120 File
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Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-20-76		OCT 27 1976	
Company Monsanto Company				Connection None		O.C.C.	
Well Burton Flat (Strawn)				Formation Strawn		Unit ARTESIA, OFFICE	
Completion Date 10-20-76		Total Depth 10572 14560		Plug Back TD 11510 11524		Elevation 3220 ft. 3241 D. F.	
Casing Size 7.00"		Casing Wt. 26.00#		Set At 6.276"		Perforations: From 10224 To 10254	
Tubing Size 2.375 NuLoc 4.70#		Tubing Wt. 1.995"		Set At 10053		Perforations: From To	
Type Well - Single - Rodenthead - G.G. or G.O. Multiple Dual Completion Gas-Gas				Packer Set At 10053		County Eddy	
Producing Thru Tubing		Reservoir Temp. *F 154 ° 10239		Mean Annual Temp. *F 60		Sero. Press. - P _a 13.2	
L 10239		H 10239		G _g 0.696		% CO ₂ 0.00	
				% N ₂ 0.00		% H ₂ S 0.00	
				Prover		Meter Run X	
				Taps			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.	
SI	87 1/2 Hrs.						2122	58		
1.	3.00		1.50	520	6.00"	72	2102	57		0.50 Hr.
2.	3.00		1.50	520	10.50"	74	2092	63		0.50 Hr.
3.	3.00		1.50	520	18.00"	74	2077	67		0.50 Hr.
4.	3.00		1.50	520	27.00"	27	2010	69		0.50 Hr.
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super. Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	11.13	56.561	533.20	0.9887	1.1987	1.0620	792
2.	11.13	74.824	533.20	0.9868	1.1987	1.0620	1046
3.	11.13	97.967	533.20	0.9868	1.1987	1.0530	1358
4.	11.13	119.985	533.20	1.0333	1.1987	1.0870	1798
5.							

NO.	P _r	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	0.80	532	1.36	0.883	29725	
2.	0.80	534	1.36	0.883	54.60	
3.	0.80	534	1.36	0.883	0.696	X X X X X X X X
4.	0.80	487	1.24	0.827	668	0.793
5.						

NO.	P _r	P _w	R _w ²	P _c ² - R _w ²
1.	2117.8	4483	76	
2.	2112.6	4463	96	
3.	2102.7	4421	138	
4.	2044.2	4179	380	
5.				

(1) $\frac{P_c^2}{P_c^2 - R_w^2} = \frac{33.03623}{33.03623 - 76} = 33.03623$

(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 33.03623$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 44863$

Absolute Open Flow	44863	Mcf @ 15.025	Angle of Slope @	45	Slope, n	1.00
Remarks:						
Approved By Commission:						
Conducted By: WEST TEXAS		Calculated By: H. L. Hagler		Checked By:		
CONSULTING SERVICE, INC.						