NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
AUG 4 1977
O. C. D.
ARTESIA, OFFICE

Type Test: ☒ Initial ☐ Annual ☐ Special		Test Date: 8-1-77	
Company: MORRIS R. ANTWEIL	Connection: None		
Pool: ~~Penn~~ Wildcat Strawn ~~Valley~~	Formation: Strawn	Unit: J	
Completion Date: 8-1-77	Total Depth: 11327	Plug Back TD: ~~11,269~~ 10110	Elevation: GL 3238
Farm or Lease Name: Mesa Fuerte Com			
Csg. Size: 5 1/2 / Wt.: 17# / d: / Set At: 11,327	Perforations: From ~~9800~~ 9822 To ~~9828~~ 9829	Well No.: 1	
Tbg. Size: 2 3/8 / Wt.: 4.7 / d: 1.995 / Set At: 9773	Perforations: From open To end	Unit: J / Sec.: 33 / Twp.: 21S / Rge.: 26E	
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 9773	County: Eddy	
Producing Thru: Tbg.	Reservoir Temp. °F: 172 @ 9773	Mean Annual Temp. °F:	Baro. Press. – P_a: 13.2
State: New Mexico			
L:	H:	Gg: .691	% CO_2:	% N_2:	% H_2S:	Prover: 6" positive choke	Meter Run:	Taps:

FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	6" positive ck.				3462	Shut-in			72 hrs.
1.	1/8	3387		76	3387				1 hr.
2.	3/16	3180		74	3180				1 hr.
3.	1/4	2180		74	2180				1 hr.
4.	5/16	1832		74	1832				1 hr.
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	.2618		3400.2	.9850	1.203	1.149	1212
2.	.6101		3193.2	.9858	1.203	1.163	2690
3.	1.112		2193.2	.9868	1.203	1.206	3492
4.	1.771		1845.2	.9868	1.203	1.196	4640
5.							

NO.	P_r	Temp. °R	T_r	Z
1.	5.08	536	1.38	.758
2.	4.77	534	1.38	.739
3.	3.28	534	1.38	.688
4.	2.76	534	1.38	.699
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas .691 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 669 P.S.I.A. _____ P.S.I.A.
Critical Temperature 388 R _____ R

P_c 3475.2 P_c^2 12077.0

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		3408.4	11617.2	459.8
2		3229.3	10428.4	1648.6
3		2270.9	5157.0	6920.0
4		2000.7	4002.8	8074.2
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 26.266$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 5.125$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 6.212$

Absolute Open Flow 6.212 Mcfd @ 15.025 | Angle of Slope θ 63.5 | Slope, n .500

Remarks: Point alignment too steep, a slope of 63.5 was drawn through low rate of flow. Well made measureable amount of fluid.

Approved by Commission:	Conducted By:	Calculated By:	Checked By:
	Reggie Burton	Reggie Burton	