File 22 file

RECEIVED
MAY 27 1977
O. C. C.
ARTESIA, OFFICE

Type Test			Test Date
[X] Initial	[ ] Annual	[ ] Special	5-10-77

Company	Connection	
GULF OIL CORP.	AIR	
Pool	**Formation**	
UNDESIGNATED	ATOKA	

Completion Date	Total Depth	Plug Back TD	Elevation	Farm or Lease Name
4-25-77	11425	10865	3336 D. F.	EDDY F.V. STATE COM.

Csg. Size	Wt.	d	Set At	Perforations:	Well No.
5.50"	17.00#	4.892"	10865	From 10377 To 10379	2
Tbg. Size	**Wt.**	**d**	**Set At**	**Perforations:**	**Unit / Sec. / Twp. / Rge.**
2.375EUE	4.70#	1.995"	10313	From To	K / 25 / 20S / 27E

Type Well – Single – Bradenhead – G.G. or G.O. Multiple	Packer Set At	County
Single Completion	10313	EDDY

Producing Thru	Reservoir Temp. °F	Mean Annual Temp. °F	Baro. Press. – P_a	State
Tubing	180 @ 10378	60	13.2	NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
10378	10378	0.638	0.42	1.41	0.00		X	

NO.	FLOW DATA: Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							3820	70			
1.	4.00		1.00	510	4.00"	106	2783	70			1.00 Hr.
2.	4.00		1.00	510	8.00"	108	1990	70			1.00 Hr.
3.	4.00		1.00	510	17.00"	115	1270	70			0.50 Hr.
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1.	4.75	45.747	523.20	0.9585	1.2519	1.0390	271
2.	4.75	64.696	523.20	0.9568	1.2519	1.0380	382
3.	4.75	94.310	523.20	0.9510	1.2519	1.0350	552
4.							
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	0.78	566	1.53	0.922
2.	0.78	568	1.54	0.922
3.	0.78	575	1.56	0.922
4.	0.78	568	1.54	0.922
5.				

Gas Liquid Hydrocarbon Ratio 5011 Mcf/Bbl.
A.P.I. Gravity of Liquid Hydrocarbons 52.80 Deg.
Specific Gravity Seperator Gas 0.638 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX 1.168
Critical Pressure 669 P.S.I.A. 650 P.S.I.A.
Critical Temperature 369 R 537 R

P_c 3833.2 P_c^2 14693

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2796.8	7822	6871
2		2003.3	4013	10680
3		1288.6	1660	13033
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.12741$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.1274$

$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 622$

Absolute Open Flow 622 Mcfd @ 15.025 Angle of Slope θ 54.00 Slope, n.000

Remarks:

Approved By: Commission Conducted By: Calculated By: Checked By: