

DATE: 5-11-78

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$$\frac{\% \text{H}_2\text{S}}{\text{MIL}}$$

T<sub>Cr</sub> 391.5  
TABLE IX A N

| LINE                                                                                      | 1       | 2       | 3       | 4       | 5       | 6 | 7 | 8 | 9 | 10 |
|-------------------------------------------------------------------------------------------|---------|---------|---------|---------|---------|---|---|---|---|----|
| 1 Q <sub>m</sub>                                                                          |         |         |         |         |         |   |   |   |   |    |
| 2 T <sub>w</sub> (W.H. °R)                                                                | 529     | 533     | 535     | 538     | 541     |   |   |   |   |    |
| 3 T <sub>s</sub> (B.H. °R)                                                                | 622     | 621     | 621     | 620     | 619     |   |   |   |   |    |
| 4 T = ( $\frac{1}{2}T_w + \frac{1}{2}T_s$ )                                               | 575.5   | 577     | 578     | 579     | 580     |   |   |   |   |    |
| 5 Z (Est.)                                                                                | .836    | .822    | .810    | .805    | .800    |   |   |   |   |    |
| 6 T <sub>Z</sub>                                                                          | 481.12  | 474.29  | 468.18  | 466.095 | 464.00  |   |   |   |   |    |
| 7 GH/TZ                                                                                   | 15.828  | 16.055  | 16.265  | 16.338  | 16.412  |   |   |   |   |    |
| 8 e <sup>s</sup> (Table XIV)                                                              | 1.8108  | 1.8259  | 1.8403  | 1.8453  | 1.8505  |   |   |   |   |    |
| 9 1-e <sup>s</sup> (Table XIV)                                                            |         | 0.4523  | 0.4566  | 0.4581  | 0.4596  |   |   |   |   |    |
| 10 P <sub>t</sub>                                                                         | 3274.2  | 3108.2  | 2967.2  | 2871.2  | 2805.2  |   |   |   |   |    |
| 11 P <sub>t</sub> 2/1000                                                                  | 10720.4 | 9660.9  | 8804.3  | 8243.8  | 7869.1  |   |   |   |   |    |
| 12 F <sub>t</sub> (Table XIV) $\frac{4H}{1000}$                                           | 59354   | 60208   | 60994   | 61267   | 61544   |   |   |   |   |    |
| 3 F <sub>c</sub> = F <sub>t</sub> TZ                                                      |         | 8.357   | 8.249   | 8.2126  | 8.1957  |   |   |   |   |    |
| 14 F <sub>c</sub> Q <sub>m</sub>                                                          |         | 8.995   | 12.406  | 16.031  | 18.738  |   |   |   |   |    |
| 15 L/H (F <sub>c</sub> Q <sub>m</sub> ) <sup>2</sup>                                      |         | 79.0    | 153.9   | 257.0   | 351.1   |   |   |   |   |    |
| 16 F <sub>w</sub> = L/H (F <sub>c</sub> Q <sub>m</sub> ) <sup>2</sup> (1-e <sup>s</sup> ) |         | 34.83   | 70.3    | 117.7   | 161.4   |   |   |   |   |    |
| 17 P <sub>w</sub> <sup>2</sup> = P <sub>t</sub> <sup>2</sup> + F <sub>w</sub>             |         | 9695.7  | 8874.6  | 8361.5  | 8030.5  |   |   |   |   |    |
| 18 P <sub>s</sub> <sup>2</sup> = e <sup>s</sup> P <sub>w</sub> <sup>2</sup>               | 19412.8 | 17703.4 | 16331.9 | 15429.5 | 14860.5 |   |   |   |   |    |
| 19 P <sub>s</sub>                                                                         | 4406    | 4207.5  | 4041.3  | 3928.0  | 3854.9  |   |   |   |   |    |
| 20 P = ( $\frac{P_t + P_s}{2}$ )                                                          | 3840.   | 3657.9  | 3504.2  | 3399.6  | 3330    |   |   |   |   |    |
| 21 P <sub>r</sub> = (P/P <sub>cr</sub> )                                                  | 5.727   | 5.455   | 5.23    | 5.070   | 4.967   |   |   |   |   |    |
| 22 T <sub>r</sub> = (T/T <sub>cr</sub> )                                                  | 1.470   | 1.474   | 1.476   | 1.479   | 1.4815  |   |   |   |   |    |
| 23 Z (Table XI)                                                                           | .836    | .822    | .810    | .803    | .800    |   |   |   |   |    |