

MEXICO OIL CONSERVATION COMM. ON
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

FEB 20 1986

Type Test ☒ Initial ☐ Annual		O. C. D. Special ARTESIA, OFFICE		Test Date 2/14/86	
Company AMOCO PRODUCTION COMPANY		Connection EL PASO NATURAL GAS COMPANY			
Pool A. BURTON FLAT WOLFCAMP		Formation WOLFCAMP		Unit	
Completion Date 8/7/78 - 2-28-83		Total Depth 11460		Plug Back TD 10065	
Elevation 3250		Farm or Lease Name STATE AC Com			
Csg. Size 5.50	Wt. 15.50	d 11485	Perforations: From 9096 To 9520		Well No. 1
Tbg. Size 2.375	Wt. 4.70	d 8990	Perforations: From - To -		Unit J
Type Well - Single - Bradenhead - G.C. or G.O. Multiple SINGLE			Packer Set At 8902		County EDDY
Producing Thru TUBING		Reservoir Temp. °F 140 @ 9250'		Mean Annual Temp. °F 60	
Baro. Press. - P _a 13.20 PSIA		State NEW MEXICO			
L 9250	H 9250	G _g 0.672	% CO ₂ 0.20	% N ₂ 0.86	% H ₂ S 0.0
Prover 0.0		Meter Run 4.0		Taps FLANGE	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w '	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							2130	62	160		120.0
1.	4.03	X	0.750	518	22.1	56	2055	64	160	64	1.0
2.	4.03	X	0.750	518	41.0	58	1922	64	160	64	2.0
3.	4.03	x	0.750	548	64.0	62	1840	65	160	65	3.0
4.	4.03	X	0.750	548	102.0	62	1823	64	160	64	4.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	2.66	108.32	531.2	1.0039	1.2199	1.0606	374
2	2.66	147.51	531.2	1.0019	1.2199	1.0596	503
3	2.66	189.52	561.2	0.9981	1.2199	1.0612	651
4	2.66	239.25	561.2	0.9981	1.2199	1.0612	322
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	0.79	516	1.36	0.839	56.108	58.0	0.672	X X X X X	668	378
2	0.79	518	1.37	0.891				X X X X X		
3	0.84	522	1.38	0.888						
4	0.84	522	1.38	0.888						
5										

P _c 2142	P _c ² 4588	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.7201$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.7808$
NO. 1	P _r ² 4277	P _w 2064	P _w ² 4261
2	3745	1932	3731
3	3434	1847	3411
4	3372	1832	3355
5			

Absolute Open Flow 2286 Mcfd @ 15.025		Angle of Slope θ		Slope, n 0.799	
Remarks:					
Approved By Commission:		Conducted By:		Calculated By:	
				Checked By: Mike Machine	

State "AC" No.1

