

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☒ Special				Test Date 2-20-81		APR 07 1981					
Company Getty Oil Company ✓				Connection Transwestern Pipeline Company		O. C. D.					
Pool South Carlsbad Wolfcamp				Formation Wolfcamp		Unit ARTESIA, OFFICE					
Completion Date 12-27-80		Total Depth 11,930'		Plug Back TD 9980'		Elevation 3266' GR					
Csg. Size 5"		Wt. 18		Set At 4.151" 11,930'		Perforations: From 9221' To 9266'					
Tbg. Size 2 3/8		Wt. 4.7		Set At 1.995" 9268'		Perforations: From To					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 8949'		County Eddy					
Producing Thru Tubing		Reservoir Temp. °F 185 @ 9291'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2					
L 8949'		H 8949'		Gg 0.712		% CO ₂ 0.95					
				% N ₂ 0.11		% H ₂ S					
				Prover		Meter Run 2"					
						Taps Flange					
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	2" X						1610		Packer		
1.	2" X 0.375			210	5	78	1400	88			1/2 hour
2.	2" X 0.375			210	10	81	1390	87			1 hour
3.	2" X 0.375			210	30	81	1365	86			1/2 hour
4.	2" X 0.375			210	55	81	1185	85			3/4 hour
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd				
1	0.6689	33.41	223.2	0.9834	1.185	1.024	27				
2	0.6689	47.24	223.2	0.9804	1.185	1.024	38				
3	0.6689	81.83	223.2	0.9804	1.185	1.024	65				
4	0.6689	110.80	223.2	0.9804	1.185	1.024	88				
5.											
NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1	0.33	538	1.37	0.954	A.P.I. Gravity of Liquid Hydrocarbons _____ No Liquids						
2	0.33	541	1.37	0.954	Specific Gravity Separator Gas .712						
3	0.33	541	1.37	0.954	Specific Gravity Flowing Fluid X X X X X						
4	0.33	541	1.37	0.954	Critical Pressure 668 P.S.I.A.						
5.					Critical Temperature 395 R						
P _c 1623.2 P _c ² 2634.8											
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.198$						
1			1997.2	637.6	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.198$						
2			1969.0	665.8							
3			1899.6	735.2							
4			1435.9	1198.9	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .193$						
5											
Absolute Open Flow 193 Mcfd @ 15.025					Angle of Slope ° 45			Slope, n 1.000			
Remarks:											
Approved By Commission:			Conducted By: Bill Krafft			Calculated By: John Murray			Checked By:		