

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 11-9-81		RECEIVED NOV 23 1981 O. C. D. ARTESIA OFFICE Government "AL"	
Company CITIES SERVICE CO. ✓		Connection TO ATMOSPHERE			
Pool BURTON FLAT		Formation ATOKA		Unit	
Completion Date 11-9-81		Total Depth 11,310		Plug Back TD 11,260	
Elevation 3272.4 GL.		Farm or Name ARTESIA		Office Government "AL"	
Csg. Size 5 1/2"	Wt. 17#	d 4.892	Set At 11,310	Perforations: From 10,843 To 10,980	
Tbg. Size 2 7/8"	Wt. 6.5#	d 2.441	Set At 10,760	Perforations: From OPEN ENDED	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple SINGLE				Packer Set At 10,760	
Producing Thru Tubing		Reservoir Temp. °F 192° @ 10,912		Mean Annual Temp. °F 60°	
Baro. Press. - P _a 13.2		State New Mexico		County EDDY	
L 10912	H 10912	Gg 0.6167	% CO ₂ .771	% N ₂ .377	% H ₂ S
Prover				Meter Run 4"	Taps Flange

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3389		PKR	CHOKE	24 HRS.
1.	4	x	1 1/2	600	12"	74	2833	58°		9/64	1 Hr.
2.	4	x	1 1/2	600	24"	67	2495	62°		11/64	1 Hr.
3.	4	x	1 1/2	610	39"	66	2077	67°		13.5/64	1 Hr.
4.	4	x	1 1/2	615	60"	76	1411	63°		16.5/64	1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	10.84	85.78	613.2	.9868	1.274	1.052	1230
2	10.84	121.31	613.2	.9933	1.274	1.055	1756
3	10.84	155.90	623.2	.9943	1.274	1.056	2261
4	10.84	194.14	628.2	.9850	1.274	1.052	2778
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	.909	534	1.47	.903	A.P.I. Gravity of Liquid Hydrocarbons 58.9 @ 60°	
2.	.909	527	1.45	.898	Specific Gravity Separator Gas 0.6167	XXXXXXX
3.	.925	526	1.45	.897	Specific Gravity Flowing Fluid XXXXX	6237
4.	.932	536	1.48	.904	Critical Pressure 674 P.S.I.A.	674 P.S.I.A.
5.					Critical Temperature 363 R	363 R

P _c 3399.7 P _c 11,557						
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.22396$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.16611$
1		2846.7	8103.7	3453.3		
2		2512.1	6310.6	5246.4		
3		2101.15	4414.8	7142.2		
4		1454.2	2114.7	9442.3		
5						

Absolute Open Flow 3,239 Mcfd @ 15.025		Angle of Slope @ 52° 45'		Slope, n 76042	
Remarks:					
Approved By Commission:		Conducted By: W.S.		Checked By: M.K.	