

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 8-18-81		SEP 14 1981																															
Company Jake L. Hamon				Location To Air																																	
Pool Undesignated				Location Morrow		Unit O. C. D. ARTESIA, OFFICE																															
Completion Date 8-14-81		Total Depth 10326		Plug Back TD 10260		Elevation 3308 Gr.																															
Csg. Size 5 1/2		Wt. 17		d 4.892		Set At 10326																															
Thq. Size 2 3/8		Wt. 4.7		d 1.995		Set At 9927																															
Perforations: From 10066 To 10087				Perforations: From Open To Ended																																	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 9927		Farm or Lease Name State 32 Com.																															
Producing Thru Tubing		Reservoir Temp. °F 183 @ 10090		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2																															
L 10090		H 10090		Gg 5982		% CO ₂ 1.328																															
						% N ₂ .398																															
						% H ₂ S -0-																															
						Prover 4"																															
						Meter Run Flange																															
FLOW DATA																																					
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Duration of Flow																														
1.	4	x	1"	460	21	73	72 Hours																														
2.	4	x	1"	470	35	95	1 Hr.																														
3.	4	x	1"	470	38	85	1 Hr.																														
4.	4	x	1"	470	45	98	1 Hr.																														
5.																																					
TUBING DATA																																					
NO.	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow																														
1.	2852		1935		7/64		1 Hr.																														
2.			1451		9.5/64		1 Hr.																														
3.			1152		11/64		1 Hr.																														
4.			568		15.5/64		1 Hr.																														
5.																																					
CASING DATA																																					
NO.	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow																														
1.																																					
2.																																					
3.																																					
4.																																					
5.																																					
RATE OF FLOW CALCULATIONS																																					
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd																														
1	4.753	99.7	473.2	.9877	1.293	1.037	628																														
2	4.753	130.0	483.2	.9680	1.293	1.033	799																														
3	4.753	135.5	483.2	.9768	1.293	1.034	841																														
4	4.753	147.5	483.2	.9653	1.293	1.031	902																														
5																																					
Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl. A.P.I. Gravity of Liquid Hydrocarbons _____ 5982 _____ Deg. Specific Gravity Separator Gas _____ XXXXXXXXXX Specific Gravity Flowing Fluid _____ XXXXXX Critical Temperature _____ °F _____ °R																																					
* $P_c = 2609.5$ $P_c^2 = 6809$ <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>NO.</th> <th>P_c^2</th> <th>P_w^2</th> <th>P_w^2</th> <th>$P_c^2 - P_w^2$</th> </tr> <tr> <td>1</td> <td></td> <td>2006</td> <td>4024</td> <td>2785</td> </tr> <tr> <td>2</td> <td></td> <td>1526</td> <td>2329</td> <td>4480</td> </tr> <tr> <td>3</td> <td></td> <td>1252</td> <td>1568</td> <td>5241</td> </tr> <tr> <td>4</td> <td></td> <td>428</td> <td>183</td> <td>6626</td> </tr> <tr> <td>5</td> <td></td> <td></td> <td></td> <td></td> </tr> </table> $(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.02762$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.01372$ $A \cdot F = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 908$								NO.	P_c^2	P_w^2	P_w^2	$P_c^2 - P_w^2$	1		2006	4024	2785	2		1526	2329	4480	3		1252	1568	5241	4		428	183	6626	5				
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4		428	183	6626																																	
5																																					
Absolute Open Flow _____ 908 _____ Mcfd @ 15.025				Angle of Slope _____ 63.5 _____		Slope, n _____ .50142																															
Remarks: * Calculated from known Bottom Hole Pressure.																																					
Approved By Commission:		Conducted By: M.R.		Calculated By: M.K.		Checked By: M.K.																															