MULTIPOINT AND ONE POINT BACK PRESSURE TEST

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O. C. D.
ARTESIA, OFFICE

File

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 12-27-84
Company: TXO Production Co.	Connection		Unit
Pool: ~~Kuster~~ East Morrow	Formation: Middle Morrow		
Completion Date: ~~12-10-84~~ 12-19-84	Total Depth: ~~11,621'~~ 11,620	Plug Back TD: ~~11,510'~~ 11,620	Elevation: ~~3119.1~~ 3119.1 GR
Farm or Lease Name: McCord "A"			
Csg. Size: 4½" / Wt.: 11.6 / d: 4.000 / Set At: ~~11,510'~~ 11,620	Perforations: From 11,460 To 11,478		Well No.: 1
Tbg. Size: 2 3/8" / Wt.: 4.7 / d: 1.995 / Set At: 10,369	Perforations: From OPEN ENDED		Unit: ~~P~~ A / Sec.: ~~19~~ 20 / Twp.: 21S / Rge.: 27E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE	Packer Set At: 10,369'		County: EDDY
Producing Thru: TUBING	Reservoir Temp. °F: 177° 10,300'	Mean Annual Temp. °F: 60°	Baro. Press. – P_a: 13.2
			State: N.M.

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
10,300	10,300	.589	1.043	.201			4.026	Flange

NO.	FLOW DATA: Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA: Press. p.s.i.g.	Temp. °F	CASING DATA: Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							1700	49°	PKR	CHOKE	72 Hours
1.	4	x	.875	760	6"	94°	1612	50		4/64	1 Hr.
2.	4	x	.875	762	16	78	1501	51		5/64	1 Hr.
3.	4	x	.875	764	32	98	1352	53		7/64	1 Hr.
4.	4	x	.875	770	57	82	1170	53		8/64	1 Hr.
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	3.630	68.11	773.2	.9688	1.303	1.047	327
2	3.630	111.37	775.2	.9831	1.303	1.055	546
3	3.630	157.70	777.2	.9653	1.303	1.047	754
4	3.630	211.29	783.2	.9795	1.303	1.054	1032
5							

NO.	P_t	Temp. °R	T_r	Z
1	1.14	554	1.59	.912
2	1.15	538	1.54	.899
3	1.15	558	1.60	.913
4	1.16	542	1.55	.900
5				

Gas Liquid Hydrocarbon Ratio: DRY Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons: Deg.
Specific Gravity Separator Gas: .589 XXXXXXXXX
Specific Gravity Flowing Fluid: XXXXX
Critical Pressure: 676 P.S.I.A. ____ P.S.I.A.
Critical Temperature: 349 R ____ R

P_c 1766.8 P_c^2 3121.6

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		1649.5	2720.8	400.8
2		1533.8	2352.5	769.1
3		1414.2	2000.0	1121.6
4		1274.0	1623.1	1498.5
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.083$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.032$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.097$

Absolute Open Flow: 2,097 Mcfd @ 15.025 | Angle of Slope θ: 46° | Slope, n: .966

Remarks: Pc and Pw calculated from known BHP, taken with a Kuster gauge.

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	S.B.	R.R.	R.R.