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State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

RECEIVED CONSERVATION DIVISION
2040 Pacheco St.
Santa Fe, NM 87505

AUG 13 1996

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator Stevens				Lease or Unit Name Bullseye			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7/8/96		Well No. 1	
Completion Date 6/29/96		Total Depth 9200		Plug Back TD 9132		Elevation 4168	
Csg. Size 5 1/2		Wt. 17		Perforations: From: 9007 To: 9027		Unit Ltr. - Sec. - TWP - Rge. H -26 -21S -22E	
Tbg. Size 2 7/8		Wt. 6.4		Perforations: From: To: 		County Eddy	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 8931		Formation Morrow	
Producing Thru Tubing L		Reservoir Temp. °F 164		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2	
L		H		Gg 0.936		% CO ₂ 36.954	
				% N ₂ 0.172		% H ₂ S 0	
				Prover		Meter Run 3.068	
						Taps FLG	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						1960		3524		
1.	3.068	0.750	520	30	60	1250	74	2797	164	1 hour
2.	3.068	0.750	490	22	60	860	74	2043	164	1 hour
3.	3.068	0.750	490	50	60	625	74	1593	164	1 hour
4.	3.068	0.750	500	27	60	500	74	1379	164	1 hour
5.										

RATE OF FLOW CALCULATIONS

NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	2.672	126.47	533.2	1.000	1.034	1.063	371
2.	2.672	105.21	503.2	1.000	1.034	1.055	307
3.	2.672	158.62	503.2	1.000	1.034	1.055	462
4.	2.672	117.71	513.2	1.000	1.034	1.056	343
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio			Dry Gas	Mcf/bbl.
1.	0.65	520	1.27	0.885	A.P. I. Gravity of Liquid Hydrocarbons			Dry	Deg.
2.	0.62	520	1.27	0.899	Specific Gravity Separator Gas			0.936	XXXXXXXXXX
3.	0.62	520	1.27	0.899	Specific Gravity Flowing Fluid			N/A	XXXXXX
4.	0.63	520	1.27	0.897	Critical Pressure			817	P.S.I.A.
5.					Critical Temperature			410	R

$P_c = 2420.3$ $P_c^2 = 5857.8$

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.289$	2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.289$
1.		1926.9	3713.0	2144.8		
2.		1441.0	2076.4	3781.4		
3.		1146.7	1315.0	4542.8		
4.		1003.2	1006.6	4851.2		
5.						

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 595$

Absolute Open Flow 595	Mcf @ 15.025	Angle of Slope Θ 45°	Slope, n 1.000
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Remarks: Well volumes fell too fast to produce conventional 4 point test. High CO₂ content could be result of acid job performed 6/28/96.

Approved By Division	Conducted By: Keltic Services	Calculated By: Jim Smith	Checked By:
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