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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MAY 27 1997

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator OXY USA, INC.					Lease or Unit Name 4 FEDERAL COM.				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 20-MAY 1997		Well No. 1		
Completion Date		Total Depth		Plug Back TD		Elevation		Unit Ltr. - Sec. - TWP - Rge.	
Csg. Size 5 1/2		Wt. d		Set At		Perforations: From: To:		County EDDY	
Tbg. Size 2 3/8		Wt. 4.7		Set At 10,762		Perforations: From: 10,848 To: 10,970		Pool Winchester Morrow	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple					Packer Set At		Formation		
Producing Thru		Reservoir Temp. °F 146		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection	
L 10,909	H 10,909	Gg 0.622	% CO ₂ 1.12	% N ₂ 0.39	% H ₂ S 0	Prover		Meter Run 3.0	Taps FLANGE

FLOW DATA

TUBING DATA

CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							3160	70			95.0
1.	3.0		1.5	369	9.3	70	3063	68			1
2.	3.0		1.5	383	19.8	54	2896	64			1
3.	3.0		1.5	392	40.8	55	2585	62			1
4.	3.0		1.5	403	71.5	48	2183	52			1
5.											

RATE OF FLOW CALCULATIONS

NO.	COEFFICIENT (24 HOUR)	$h_w P_m$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.		59.60	382.0	0.9910	1.2680	1.0327	827
2.		88.60	396.5	0.9959	1.2680	1.0352	1211
3.		128.58	405.2	1.0044	1.2680	1.0384	1874
4.		172.51	416.2	1.0114	1.2680	1.0416	2396
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P. I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.57	530	1.46	0.938	56.5	56.7	0.622	XXXXXX	676	362
2.	0.59	524	1.45	0.933						
3.	0.60	516	1.42	0.927						
4.	0.62	508	1.40	0.922						
5.										

P_c 3160.6 P_c² 9989

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1.	9460	3070	9427	562
2.	8465	2913	8485	1504
3.	6751	2617	6848	3142
4.	4823	2244	5035	4955
5.				

$$1) \frac{P_c^2}{P_c^2 - P_w^2} = 2.0162 \quad (2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.4199$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3402$$

Absolute Open Flow **3402** Mcfd @ 15.025 Angle of Slope θ **63.4** Slope, n **0.50**

Remarks:

Approved By Division

Conducted By:

Larry Davis by [Signature]

Calculated By:

Checked By: