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State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator <u>OXY USA, INC.</u>					Lease or Unit Name <u>BULLDOG</u>				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date <u>19-MAY-97</u>		Well No. <u>1</u>		
Completion Date		Total Depth		Plug Back TD <u>11,040</u>		Elevation		Unit Ltr. - Sec. - TWP - Rge.	
Csg. Size <u>4 1/2</u>	Wt. <u>d</u>	Set At	Perforations: From <u>10,874</u> To <u>11,154</u>			County <u>EDDY</u>			
Tbg. Size <u>NONE</u>	Wt. <u>d</u>	Set At	Perforations: From <u></u> To <u></u>			Pool <u>BURTON Flat MORROW</u>			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple					Packer Set At		Formation		
Producing Thru <u>147</u>		Reservoir Temp. °F <u>60</u>		Baro. Press - P _a <u>13.2</u>		Connection			
L <u>11,014</u>	H <u>11,014</u>	Gg <u>0.625</u>	% CO ₂ <u>0.45</u>	% N ₂ <u>1.08</u>	% H ₂ S <u>0</u>	Prover	Meter Run <u>3.0</u>	Taps <u>FLANGE</u>	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI									<u>3160</u>	<u>70</u>	<u>72.0</u>
1.	<u>3.02</u>		<u>1.250</u>	<u>337</u>	<u>13.3</u>	<u>57</u>			<u>3090</u>	<u>57</u>	<u>1</u>
2.	<u>3.02</u>		<u>1.250</u>	<u>341</u>	<u>26.4</u>	<u>48</u>			<u>2985</u>	<u>60</u>	<u>1</u>
3.	<u>3.02</u>		<u>1.250</u>	<u>340</u>	<u>50.3</u>	<u>37</u>			<u>2846</u>	<u>52</u>	<u>1</u>
4.	<u>3.02</u>		<u>1.250</u>	<u>353</u>	<u>105.3</u>	<u>26</u>			<u>2569</u>	<u>49</u>	<u>1</u>
5.											

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.		<u>68.20</u>	<u>349.7</u>	<u>1.0025</u>	<u>1.2649</u>	<u>1.0328</u>	<u>674</u>
2.		<u>96.63</u>	<u>353.7</u>	<u>1.0117</u>	<u>1.2649</u>	<u>1.0354</u>	<u>995</u>
3.		<u>133.29</u>	<u>353.2</u>	<u>1.0229</u>	<u>1.2649</u>	<u>1.0383</u>	<u>1371</u>
4.		<u>197.30</u>	<u>366.2</u>	<u>1.0344</u>	<u>1.2649</u>	<u>1.0432</u>	<u>2111</u>
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	<u>0.52</u>	<u>517</u>	<u>1.43</u>	<u>0.938</u>	<u>74.3</u>	
2.	<u>0.53</u>	<u>508</u>	<u>1.40</u>	<u>0.933</u>	<u>62.6</u>	
3.	<u>0.53</u>	<u>497</u>	<u>1.37</u>	<u>0.928</u>		
4.	<u>0.55</u>	<u>486</u>	<u>1.34</u>	<u>0.919</u>		
5.						

NO.	P _c	P _w	P _w ²	P _c ² - P _w ²
1.	<u>9630</u>	<u>3096</u>	<u>9583</u>	<u>409</u>
2.	<u>8989</u>	<u>3001</u>	<u>9008</u>	<u>983</u>
3.	<u>8176</u>	<u>2875</u>	<u>8267</u>	<u>1724</u>
4.	<u>7193</u>	<u>2703</u>	<u>7305</u>	<u>2686</u>
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{3.7192}$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{4679}$

2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{2.2158}$

Absolute Open Flow <u>4679</u>	Mcf/d @ 15.025	Angle of Slope θ <u>58.8</u>	Slope, n <u>0.606</u>
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Remarks:

Approved By Division

Conducted By:

Calculated By:

Checked By:

Larry Davis by M

R. J. Backhammer