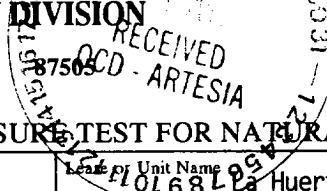


Submit in duplicate to
appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION
2040 Pancheco St.
Santa Fe, NM 87505



MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR NATURAL GAS WELL

Operator <u>R.C. Bennett</u>					Unit Name <u>La Huerta 32</u>				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date <u>4/20/01</u>		Well No. <u>1-Y</u>		
Completion Date <u>2/26/01</u>		Total Depth <u>11,777'</u>		Plug Back TD <u>11,642'</u>		Elevation <u>3109'</u>		Unit Ltr. - Sec. - TWP - Rge. <u>32 21S 27E</u>	
Csg. Size <u>8-5/8"</u>	Wt. <u>32#</u>	d	Set At <u>2806'</u>	Perforations: From: <u>11,379'</u> To: <u>11,440'</u>			County <u>Eddy</u>		
Csg. Size <u>4-1/2"</u>	Wt. <u>11.6#</u>	d	Set At <u>11,760'</u>	Perforations: From: To:			Pool <u>Burton Flat</u>		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple <u>Single</u>				Packer Set At			Formation <u>Morrow</u>		
Producing Thru <u>Pipeline</u>		Reservoir Temp. °F		Mean Annual Temp. °F		Baro. Press - P _a		Connection <u>El Paso</u>	
L	H	Gg	%CO ₂	%N ₂	H ₂ S	Prover	Meter Run	Taps	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size X	Orifice Size	Press p.s.i.g	Diff. h _w	Temp. °F	Press p.s.i.g	Temp. °F	Press p.s.i.g		Temp. °F
SI	3.067 X 0					2175	94			-
1.	3.067 X 7/64					2153	77			2
2.	3.067 X 13/64					2071	72			2
3.	3.067 X 19/64					1758	77			2
4.	3.067 X 21/64					1617	66			2
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	Elec. flow mtr						1219
2.	Elec. flow mtr						2093
3.	Elec. flow mtr						4497
4.	Elec. flow mtr						5063
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					A.P.I Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas <u>0.602</u>	<u>XXXXXXXXXX</u>
3.					Specific Gravity Flowing Fluid <u>XXXXX</u>	
4.					Critical Pressure <u>671.49</u> P.S.I.A.	P.S.I.A.
5.					Critical Temperature <u>357.13</u> R	R

P _c <u>2190</u>		P _c ² <u>4796.2</u>		1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{2.249}{\quad}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \frac{1.59}{\quad}$	
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²			
1.		2168	4700.3	95.9			
2.		2086	4351.5	444.7			
3.		1773	3143.6	1652.6			
4.		1632	2663.5	2132.7			
5.							

Absolute Open Flow <u>8048.8</u> Mcfd @ 15.025		Angle of Slope Θ <u>60.25</u>		Slope, n <u>0.572</u>	
Remarks: <u>✓</u>					
Approved by Commission:		Conducted by:		Calculated by:	
				Checked by:	