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appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources

Form C-122
Revised October, 1999

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OCD - ARTESIA
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator BONNEVILLE FUELS						Lease or Unit Name LAKESHORE 10 COM					
Type Test ☐ XX Initial ☐ Annual ☐ Special						Test Date 09/24/01		Well No. #4			
Completion Date 8-1-2001		Total Depth 11124		Plug Back TD 10495		ELEVATION 3229		Unit Ltr. - Sec. - TWP - Rge D 10 21S 26E			
Csg. Size 4.5	Wt. 11.6	D 4.0	Set At 11120	Perforations: SANDS From: To: 9663 To: 9713				County EDDY			
Thg. Size 2.375	Wt. 4.7	D 1.99	Set At 9759	Perforations: LIME From: 9772 To: 9788				Pool AVALON STRAWN			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single SINGLE						Packer Set At N/A		FORMATION STRAWN FM			
Producing Thru Tubing		Reservoir Temp. °F 160		Mean Annual Temp. °F		Baro. Press - P _s 15.2		Connect on Pipeline			
L	H	Gg 0.6906	%C 1.2679	%N ₂ 1.2834	%H ₂ S 0.0	Prover		Material 4 inch	Taps Flange		

FLOW DATA						TUBING DATA		CASING DATA		Duration Of Flow
No.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	4					1100				137 hrs
1.	4	2.00	547	1.69	79	950				1 Hour
2.	4	1.125	563	32.5	74	820				1 Hour
3.	4	1.125	562	49.0	73	700				1 Hour
4.	4	1.125	561	53.3	74	580				1 Hour
5.										

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compres. Factor F _{pv}	Rate of Flow Q, Mcfd
1.	23.18	30.8	560.2	0.9822	1.2033	1.0574	891
2.	6.332	136.8	576.2	0.9868	1.2033	1.0614	1092
3.	6.332	167.9	575.2	0.9877	1.2033	1.0617	134
4.	6.332	174.9	574.2	0.9868	1.2033	1.0611	1396
5.							

No.	P _r	Temp. °R	T _r	Z	Gas - Liquid Hydrocarbon Ratio	Mcf/bbl.
1.					A. P. I. Gravity of Liquid Hydrocarbons	Deg.
2.					Specific Gravity Separator Gas XXXXXXXXXX	
3.					Specific Gravity Flowing Fluid XXXXXX	
4.					Critical Pressure _____ P.S.I.A.	P.S.I.A.
5.					Critical Temperature _____ R.	R

P _c 1150.2		P _c ² 1323	
No.	P _r ²	P _w ²	P _c ² - P _w ²
1.	1035.8	1072.9	250.1
2.	929.5	864.0	459.0
3.	853.4	728.3	594.7
4.	758.8	575.8	747.2
5.			

(1) $P_c^2 = 1150.2$ (2) $P_c^2 = 1323$

$\frac{P_c^2 - P_w^2}{P_c^2 - P_w^2}$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1801 \text{ MCF}$

Absolute Open Flow 1801	Mcf/d @ 15.025	Angle of Slope θ 65.9	Slope, n: 0.45
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Remarks: **Choke Sizes: Q₁=9/64 Q₂= 12/64 Q₃=14/64 Q₄= 20/64**

Approved By Division	Conducted By: KELTIC SERVICES	Calculated By: LARRY MOSSBARGER	Checked By:
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CAOF PLOT

