

RECEIVED

NEW MEXICO OIL CONSERVATION COMMISSION

MAY 16 1966

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS  
ARTESIA, OFFICE

Pool Wildcat Formation Pennsylvanian County 7 21 Bddy

Initial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 11/28/58

Company Tennessee Gas Transmission Co. Lease State John M. Kelly "B" Well No. 1

Unit N Sec. 27 Twp. 24-S Rge. 27-E Purchaser None

Casing 9 5/8 Wt. 47.0 I.D. 8 1/8 Set at 10,652' Perf. None To \_\_\_\_\_

Tubing 2 3/8 Wt. 4.7 I.D. 2 1/8 Set at 11,550 Perf. \_\_\_\_\_ To \_\_\_\_\_

Gas Pay: From 10,652 To 12,655 L 11,550' xG .635 -GL 7334 Bar.Press. 13.2

Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well Single

Date of Completion: 11/4/58 Packer 10,550 Single-Bradenhead-G. G. or G.O. Dual Reservoir Temp. 192° F

OBSERVED DATA

Tested Through (Flow) (Choke) (Flow) Type Taps \_\_\_\_\_

No.	Flow Data				Tubing Data		Casing Data		Duration of Flow Hr.	
	(Line) Size	(Choke) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig		Temp. °F.
SI						4400	60			78
1.	2"	8/8"	590		60	590	60			8
2.	2"	1 1/8"	315		60	315	60			14
3.										
4.										
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	.3261		603.2	1.000	.9721	1.059	202.5
2.	.6224		328.2	1.000	.9721	1.029	204.3
3.							
4.							
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio -- cf/bbl.  
 Gravity of Liquid Hydrocarbons -- deg.  
 F<sub>c</sub> 9.936 (1-e<sup>-s</sup>) .396  
 Specific Gravity Separator Gas .635  
 Specific Gravity Flowing Fluid --  
 P<sub>c</sub> 4413 P<sub>c</sub><sup>2</sup> 19,475

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> P <sub>c</sub>
1.	603.2	364	2012	4046	1603	1967	17,908	1402 <sup>w</sup>	.326
2.	328.2	108	2030	4121	1632	1740	17,733	1319	.299
3.					Point 1	365.6	19,109.4	624.2	.137
4.					Point 2	107.6	19,365.4	331.1	.075
5.									

Absolute Potential: 2.8 2.18 MCFPD; n 0.72

COMPANY Tennessee Gas Transmission Company

ADDRESS Box 307, Hobbs, New Mexico

AGENT and TITLE J. F. Carnes J. F. Carnes, District Engineer

WITNESSED \_\_\_\_\_

COMPANY \_\_\_\_\_

REMARKS

Shut-in gas well - no pipe line connection.

*[Handwritten signature]*

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressibility factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .