

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

RECEIVED
Revised 9-1-65

DEC 23 1969

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 12-11-69		O. C. C. ARTERIA, OFFICE					
Company Texas American Oil Corporation			Connection None						
Pool Wildcat			Formation Atoka						
Completion Date 12-12-69		Total Depth 16,486		Plug Back TD 14,950					
Elevation 3437 GL		Farm or Lease Name Todd Federal "26"							
Csq. Size 7 5/8	Wt. 39.00	d 16,486	Set At 16,486	Perforations: From 13,679 To 13,907					
Trq. Size 3 1/2	Wt. 10.3	d 3,500	Set At 13,614	Perforations: From To					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 13,600					
Producing Thru Tubing		Reservoir Temp. *F 214		Mean Annual Temp. *F 13.2					
L 13,614		H 13,614		Gg .594					
% CO ₂ Nil		% N ₂ Nil		% H ₂ S .21					
Prover 6		Meter Run 6		Taps Flange					
FLOW DATA			TUBING DATA		CASING DATA				
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. *F	Press. p.s.i.g.	Temp. *F	Duration of Flow
SI									
1.	6	X	2.500	875	12	58	7778	74	60 min.
2.	6	X	2.500	885	27	63	7693	80	60 min.
3.	6	X	2.500	885	51	64	7563	83	60 min.
4.	6	X	2.500	890	72	61	7427	86	60 min.
5.									
RATE OF FLOW CALCULATIONS									
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd		
1	30.44	103	888.2	1.002	1.298	1.03177	4407		
2	30.44	156	893.2	.9971	1.298	1.07977	6632		
3	30.44	214	893.2	.9962	1.298	1.07677	9063		
4	30.44	255	903.2	.9990	1.298	1.08577	10921		
5									
NO.	P _r	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio None Mcf/bbl.				
1	1.22	512	1.44	0.81	A.P.I. Gravity of Liquid Hydrocarbons Deg.				
2	1.22	512	1.44	0.81	Specific Gravity Separator Gas .594 XXXXXXXXXX				
3	1.34	521	1.48	0.81	Specific Gravity Flowing Fluid XXXXX				
4	1.34	521	1.48	0.81	Critical Pressure 172 P.S.I.A. P.S.I.A.				
5					Critical Temperature 354 R R				
NO.	P _r	P _w	R _r	P _r ² - R _w ²	(1) $\frac{P_r^2}{P_r^2 - R_w^2} = 12.012$ (2) $\left[\frac{P_r^2}{P_r^2 - R_w^2} \right]^n = 6.75$				
1	USED	9664.2	93397		AOF = Q $\left[\frac{P_r^2}{P_r^2 - R_w^2} \right]^n = 73305$				
2	SUB-	9540.2	91015	2382					
3	SURFACE	9463.2	89552	3845					
4	AMERADA	9343.2	87295	6102					
5	GAUGE	9253.2	85622	7775					
Absolute Open Flow 75,000 Mcfd @ 15.025					Angle of Slope 52.5		Slope, n .767		

Remarks: From small, direct liquid out 2%

Prepared By: Roy E. Valla
Checked By: Roy E. Valla
Company: Pom Harrison Company
Location: Richard Thomas