

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 2/23/70		MAR 3 1970		
Company Gulf Oil Corporation					Connection None				
Pool Rock Tank					Formation Lower Morrow		Unit ARTESIA, OFFICE		
Completion Date 2/18/70		Total Depth 10,350		Plug Back TD 10,312		Elevation 4008 GL		Farm or Lease Name Boothe "B0" Federal	
Csg. Size 5 1/2	Wt. 17#	d 4.892	Set At 10,314	Perforations: From 10,230 To 10,262		Well No. 1			
Tbg. Size 2 7/8	Wt. 6.5#	d 2.441	Set At 10,180	Perforations: From _____ To _____		Unit K Sec. 12 Twp. 23S Rge. 24E			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual Gas-Gas					Packer Set At 10,180		County Eddy		
Producing Thru Tubing		Reservoir Temp. *F 156@ 10,250		Mean Annual Temp. *F 60°		Baro. Press. - P _a 13.2		State New Mexico	
L 10,180	H 10,180	Gg .582	% CO ₂ 0.53%	% N ₂ 0.30%	% H ₂ S -	Prover	Meter Run X	Taps Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. *F	Press. p.s.i.g.	Temp. *F	Press. p.s.i.g.		Temp. *F
SI							3116		Check		73.25
1.	6	X	1.75	610	10	102	2470	65	10/64		1.5
2.	6	X	1.75	620	15.5	94	2300	65	12/64		1.0
3.	6	X	1.75	638	29	89	1823	65	15/64		1.25
4.	6	X	1.75	642	59	76	1220	65	17/64		2.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	14.61	78.94	623.2	.918	1.311	1.036	1507
2	14.61	99.07	633.2	.940	1.311	1.039	1910
3	14.61	137.4	651.2	.973	1.311	1.043	2671
4	14.61	181.0	655.2	.983	1.311	1.047	3575
5.							

NO.	P _t	Temp. *R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.	0.93	562	1.61	.931	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	0.94	554	1.59	.926	Specific Gravity Separator Gas .582 XXXXXXXXXX
3.	0.97	549	1.57	.919	Specific Gravity Flowing Fluid XXXXXX
4.	0.97	536	1.54	.912	Critical Pressure 674 P.S.I.A. P.S.I.A.
5.					Critical Temperature 349 R R

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.2016$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.2016$ $AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4296$
1		2487.8	6189.1	3615.3	
2		2320.5	5384.7	4419.7	
3		1854.6	3439.5	6364.9	
4		1282.6	1645.1	8159.3	

Absolute Open Flow 4296 Mcfd @ 15.025		Angle of Slope @ _____		Slope, n 1.000
Remarks: _____				
Approved By Commission: 3-4-70 Conducted By: H. L. Smith Calculated By: Dennis Holley Checked By: H. L. Smith				