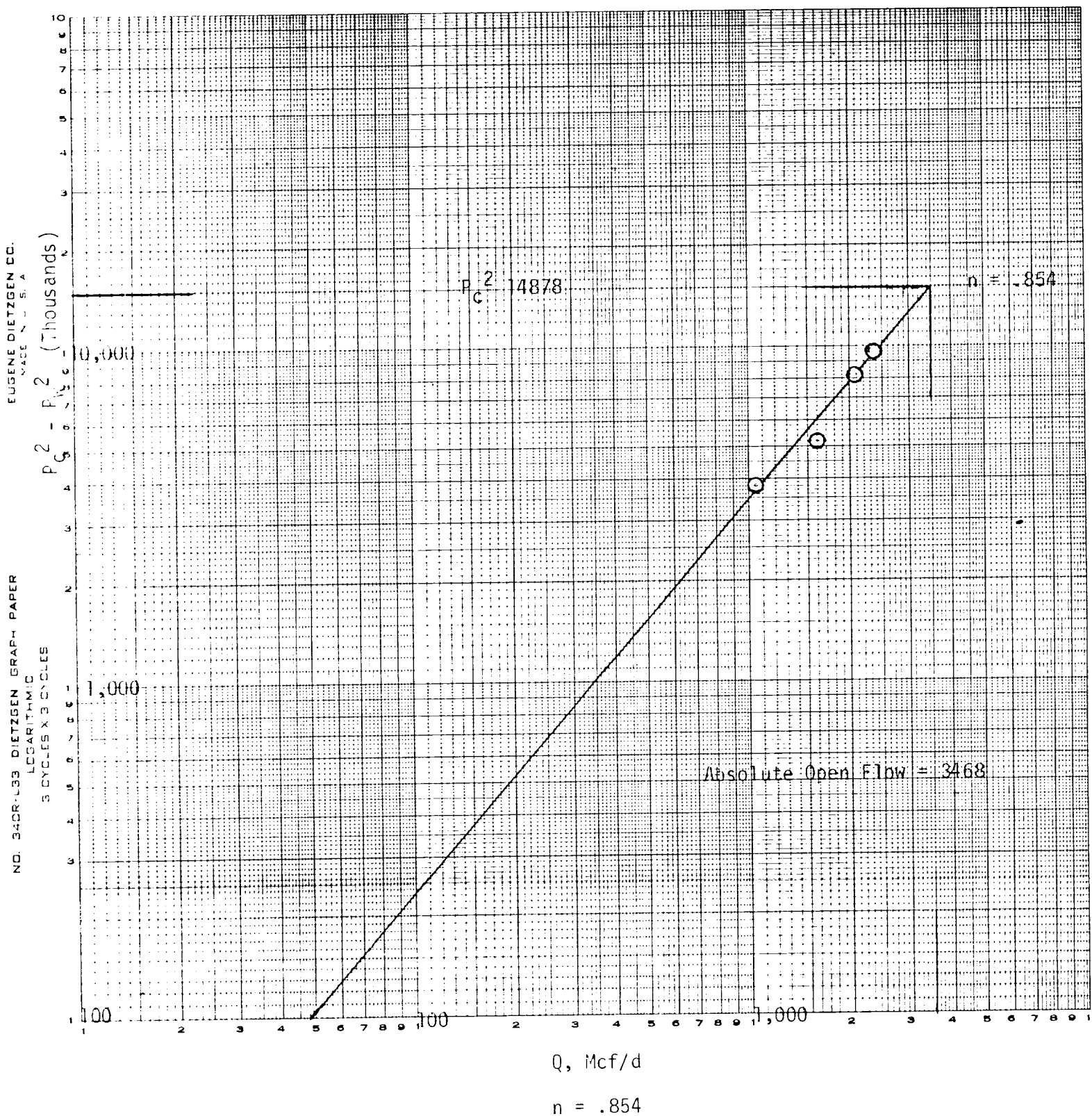


Company : Morris R. Antw
 Well : Allen No. 1-LT
 Location : 31 - 22S - 27E
 County : Eddy
 Date : 10-3-70



NE MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 10-1-65
RECEIVED

JAN 14 1971

Type of Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-3-70		O. D. D. ARTESIA, OFFICE	
Company Morris R. Antweil				Connection None			
Pool Wildcat <i>Morrow</i>				Formation Morrow		Unit	
Completion Date 10-3-70		Total Depth 11,825		Plug Back TD 11,614		Elevation 3204 DF	
Form or Lease Name Allen		Well No. 1-LT		Unit 31		Sec. Twp. Rge. 22-S 27-E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G. G. Multiple (Dual)		Packer Set At 11,370		County Eddy		State New Mexico	
Producing Thru Tubing		Reservoir Temp. °F 195 @ 11,452		Mean Annual Temp. °F 13.2		Baro. Press. - P _a	
L 11452		H 11452		G _g .598		% CO ₂ % N ₂ % H ₂ S Prover	
						Meter Run 3"	
						Flange	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3844	60	Pkr.		+72 Hrs.
1.	3.068	x	1.500	807	6.5	118	3303	72			1 Hr.
2.	3.068	x	1.500	851	14.0	103	2967	72			.75 Hr.
3.	3.068	x	1.500	810	24.5	100	2518	72			.75 Hr.
4.	3.068	x	1.500	807	32.0	96	2204	72			.75 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor F _{pv}	Rate of Flow Q, Mcfd
1	11.13	73.02	820.2	.9485	1.293	1.046	1043
2	11.13	110.0	864.2	.9610	1.293	1.054	1603
3	11.13	142.0	823.2	.9636	1.293	1.053	2074
4	11.13	162.0	820.2	.9671	1.293	1.054	2377
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Dry	Mcf/bbl.
1	1.22	578	1.63	.914	A.P.I. Gravity of Liquid Hydrocarbons	---	Deg.
2	1.29	563	1.59	.900	Specific Gravity Separator Gas	.598	X X X X X X X X
3	1.23	560	1.58	.902	Specific Gravity Flowing Fluid	X X X X X	.598
4	1.22	556	1.57	.900	Critical Pressure	672	P.S.I.A. 672 P.S.I.A.
5					Critical Temperature	354	R 354 R

P _c 3857.2 P _c ² 14878				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{14878}{9597}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.459$	
NO.	P _w	P _w ²	P _c ² - P _w ²	ACF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3468$			
1	3328.2	11077	3801				
2	3109.8	9671	5207				
3	2586.3	6689	8189				
4	2298.0	5281	9597				
5							

Absolute Open Flow		3468	Mcf/d @ 15.025	Angle of Slope		49.5°	Slope, n	.854
Remarks:								
Approved By Commission:			Conducted By:		Calculated By:		Checked By:	
			Bill Kerley		Larry Cone		Larry Cone	