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O. C. C.
ARTESIA, OFFICE

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NEW MEXICO OIL CONSERVATION COMMISSION
Form C-122
Revised 1-1-65

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELLS

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 9-21-72	
Company: TEXACO Inc.			Connection: -		
Pool: White City			Formation: Morrow		Unit:
Completion Date: 9-21-72	Total Depth: 11,540		Plug Back TD: 11,250	Elevation: 3413	Farm or Lease Name: New Mex. "DD" St.Com
Csg. Size: 4.5	Wt.: 11.6 / 13.5	d: 4.00 / 3.92	Set At: 11540	Perforations: From 11090 To 11166	Well No.: 1
Tbg. Size: 2 3/8	Wt.: 4.7	d: 1.99	Set At: 10974	Perforations: From To	Unit: G; Sec.: 32; Twp.: 24; Rge.: 26
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single Gas			Packer Set At: 10974		County: Eddy
Producing Thru: Tubing	Reservoir Temp. °F: 174 @11253		Mean Annual Temp. °F:	Baro. Press. – P_a: 13.2	State: New Mexico

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
10974	10974	0.576	0.9	0.2	0.0		4.067	Flg

	FLOW DATA				TUBING DATA		CASING DATA		
NO.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI					3912	60			46
1.	4 x 2.00	202.2	4.0	100	3537	74			1
2.	4 x 2.00	237.7	9.6	78	3150	72			1
3.	4 x 2.00	331.2	13.0	58	2579	72			1
4.	4 x 2.00	439.2	17.6	78	1731	72			1
5.									

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	1981	29.4	215.4	0.9636	1.318	1.013	748
2.	1981	49.1	250.9	0.9831	1.318	1.018	1283
3.	1981	66.8	344.4	1.0019	1.318	1.029	1798
4.	1981	89.3	452.5	0.9831	1.318	1.033	2369
5.							

NO.	P_t	Temp. °R	T_r	Z
1.	0.32	560	1.59	0.974
2.	0.37	538	1.53	0.964
3.	0.51	518	1.47	0.944
4.	0.67	538	1.53	0.937
5.				

Gas Liquid Hydrocarbon Ratio 0.0 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons - Deg.

Specific Gravity Separator Gas	0.576	xxxxxxxxx
Specific Gravity Flowing Fluid	xxxxx0.576	
Critical Pressure	678 P.S.I.A.	678 P.S.I.A.
Critical Temperature	352 R	352 R

P_c 3925 P_c^2 15407.2

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	12604	3553	12627	2780
2	10006	3172	10062	5346
3	6720	2611	6818	8590
4	3042	1790	3204	12203
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{15407}{12139} = 1269^{(2)}$ $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.203$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2849$

Absolute Open Flow 2849 Mcfd @ 15.025 | Angle of Slope θ 52.2 | Slope, n 7746

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Lee	Computer	