

NEW MEXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

PLEASE NOTE: CORRECTED C-122

Type Test		☒ Initial ☐ Annual ☐ Special		Test Date 4/4/97							
Company Mallon Oil Company			Connection LG & E								
Pool <i>S Carlisle Morrow</i> White City			Formation Morrow		Unit <i>11-24-26</i>						
Completion Date 3/18/97		Total Depth 11,900		Plug Back TD 11,480	Elevation 3,319 KB						
Csg. Size 5-1/2"		Wt. 17 and 20#	d 4,778	Set At 11,904	Perforations: From 11,198 To 11,206						
Tbg. Size 2-3/8"		Wt. 4.7#	d 1.995	Set At 11,098	Perforations: From To						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single Completion				Packer Set At 11,098	Well No. 1						
Producing Thru Tubing		Reservoir Temp. ° F 189	Mean Annual Temp. ° F 60	Baro. Press. - P _a 13.2	Farm or Lease Name O'Neill Federal						
L 11,202	H 11,202	Gg .676	% CO ₂ 0.0	% N ₂ 2.49	% H ₂ S 0.0						
Provor		Meter Run 4"	Taps Flange								
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. ° F	Press. p.s.i.g.	Temp. ° F	Press. p.s.i.g.	Temp. ° F	Duration of Flow
SI							3950		PKR		
1.	4.026 x 2.5			540	0.3	75	3850	70			1
2.	4.026 x 2.5			547	0.8	98	3350	70			1.083
3.	4.026 x 2.5			552	1.4	97	2740	68			1.083
4.	4.026 x 2.5			557	2.1	97	1950	64			1.25
5.	4.026 x 2.5										
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd				
1.	32.64	12.9	554	.9859	1.216	1.057	533				
2.	32.64	21.2	560	.9653	1.216	1.044	847				
3.	32.64	28.1	565	.9662	1.216	1.045	1127				
4.	32.64	34.6	570	.9662	1.216	1.045	1387				
5.											
NO.	P _r	Temp. ° R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.						
1.	.832	535	1.423	.895	A.P.L. Gravity of Liquid Hydrocarbons _____ Deg.						
2.	.841	558	1.484	.917	Specific Gravity Separator Gas _____ XXXXXXXX						
3.	.848	557	1.481	.916	Specific Gravity Flowing Fluid _____ XXXX .676						
4.	.856	557	1.481	.915	Critical Pressure _____ P.S.I.A. _____ P.S.I.A.						
5.					Critical Temperature _____ R _____ R						
P _c 3963		P _c 15707									
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.34$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.158$				
1.	14924	3866	14947	760							
2.	11311	3371	11365	4342							
3.	7580	2769	7670	8037							
4.	3854	1996	3984	11723							
5.											
Absolute Open Flow 1606					Mcf/d @ 15.025			Angle of Slope		Slope, n .50	
Remarks:											
Approved by Commission:											
Conducted By: TL				Calculated By: REJ				Checked By:			