

RECEIVED

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ARTESIA OFFICE ☒ Initial ☐ Annual ☐ Special		Test Date 11/5/70	
Company BYRON M. McKNIGHT		Connection Pending	
Pool		Formation Atoka	
Completion Date 11/15/70		Total Depth ?	
Perforations: From 10,608 To 10,618		Elevation ?	
Farm or Lease Name Grandi Ranch		Well No. 1	
Ceq. Size 5 1/2"	Wt. 20	d 4.778	Set At ?
Thq. Size 2 3/8"	Wt. 4.7	d 1.995	Set At ?
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At 10,500	
Producing Thru Tubing		Reservoir Temp. °F 60	
Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
State New Mexico		County Eddy	
L 1.500 ?	H	G _q .612	% CC ₂ .60
% N ₂ .56		% H ₂ S 0	
Prover 2"		Meter Run 2"	
Taps			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							864	60	Packer		15 days
1.	2.00 x 3/32			397 849	.37	73	849	60	"		1 hour
2.	2.00 x 3/16			413 823	.75	76	823	60	"		"
3.	2.00 x 1/4			397 761	1.21	73	761	60	"		"
4.	2.00 x 5/16			397 704	1.62	70	704	60	"		"
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	.1410	7.73	410.2	.9877	1.278 1.260	1.037 34	207 75
2	.6082	15.75	426.2	.9850	"	1.036 34	414 337
3	1.087	25.24	410.2	.9887	"	1.037 34	666 582
4	1.672	33.73	410.2	.9905	"	1.037 36	890 377
5.							

NO.	F _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcfd/bbl.
1	.61	533	1.45 1.48	.9305	A.P.I. Gravity of Liquid Hydrocarbons	
2	.63 .64	536	1.46 1.47	.9295	Specific Gravity Separator Gas	XXXXXXX
3	.61	533	1.45 1.48	.9305	Specific Gravity Flowing Fluid	XXXXX
4	.61	530	1.45 1.47	.9302	Critical Pressure 615	P.S.I.A.
5					Critical Temperature 360	R

NO.	F _r	P _w	P _w ²	P _c ² - P _w ²
1	Used	1124.2	1263.8	43.1
2	Amerada	1090.2	1188.5	118.4
3	Bomb	1008.2	1016.5	290.4
4		937.2	878.3	428.6
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.049$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2104$

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.341$

Absolute Open Flow	1,790 2100	Mcfd @ 15.025	Angle of Slope θ	56.5	Slope, n	763 .662
Remarks:						
Approved By Commission:		Conducted By:		Calculated By:		Checked By: