

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST

Form G-122
Revised 9-1-65

221972

Type Test ☐ Initial ☒ Annual ☐ Special					Test Date 1-11-72				
Company CITIES SERVICE OIL COMPANY				Connection Transwestern Pipeline Co.				Office LAWRENCE OFFICE	
Pool South Carlsbad				Formation Morrow				Unit 8	
Completion Date 12-18-70		Total Depth 11,841		Plug Back TD 11,795		Elevation		Farm or Lease Name Strackbein "A"	
Csg. Size 5 1/2"	Wt. 17 & 20#	d 4.778	Set At 11,825	Perforations: 11763 11773 From 11400 To 11480		Well No. 1			
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 11310	Perforations: From To		Unit E		Sec. Twp. Rge. 32 22S 27E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 11310		County Eddy		
Producing Thru Tubing		Reservoir Temp. °F 178° 11840		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State New Mexico	
L 11310	H 11310	Gg .58	% CO ₂ 1.04	% N ₂ .24	% H ₂ S --	Prover Orifice	Meter Run 2"	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	BHP p.s.i.g.		Temp. °F
SI	24 hrs.						3024		3912		
1.	2 x 1,375			975	3	73	2960		3799		1 hr.
2.	2 x 1,375			980	7.5	74	2910		3736		1 hr.
3.	2 x 1,375			990	21	77	2771		3611		2 hrs.
4.	2 x 1,375			925	52	76	2410		3209		3 1/2 hrs.
5.	72 hrs. S.I.						3428		4389		

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor Fpv	Rate of Flow Q, Mcfd
1	10.20	54.45	988.2	.9877	1.313	1.071	771
2	10.20	86.31	993.2	.9868	1.313	1.071	1222
3	10.20	145.15	1003.2	.9840	1.313	1.070	2047
4	10.20	220.88	938.2	.9850	1.313	1.066	3106
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	1.46	533	1.53	.871			.580		672	350
2	1.47	534	1.53	.871						
3	1.48	537	1.54	.873						
4	1.39	536	1.54	.880						
5										

P _c 3925.2 P _c ² 15,407.2				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 6.78$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6.51$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 13,326$		
1		3812.2	14532.9	874.3	Point 3		
2		3749.2	14056.5	1350.7			
3		3624.2	13134.8	2272.4			
4		3222.2	10382.6	5024.6			
5							

Absolute Open Flow 13,326 Mcfd @ 15.025		Angle of Slope 0		Slope, n .98	
Remarks: P _w taken from BHP bomb.					
Approved By Commission:		Conducted By: Bennett & Nichols		Calculated By: Nichols	
				Checked By: Bennett	