

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7/28/71		AUG 10 1971	
Company Corinne Grace				Connection None			
Pool South Corlebed <i>Marrow</i>				Formation Marrow		Unit O. C. C. ARTESIA, OFFICE	
Completion Date 6/20/71		Total Depth 12,011		Plug Back TD 11,945		Elevation 3250 OL	
Csg. Size 7" 1 1/2		Wt. 29# 13.54		Perforations: From 11680 To 11690		Well No. 1	
Tbg. Size 2 3/8		Wt. 4.70		Perforations: From To		Unit Sec. Twp. Rge. P 2 238 26E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 10,616		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 167 @ 10,616		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2	
L 10,616		H 10,616		Gg .580		% CO ₂ % N ₂ % H ₂ S Prover Meter Run Taps - - - I Flg	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3475	70			72
1.	3	X	2.25	640	10	74	3370	70			1
2.	3	X	2.25	675	20	55	3255	70			1
3.	3	X	2.25	705	40	54	3043	70			1
4.	3	X	2.25	780	80	43	2538	70			1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	28.78	80.82	653.2	.9868	1.313	1.048	3158
2	28.78	117.32	688.2	1.005	1.313	1.059	4718
3	28.78	169.49	718.2	1.006	1.313	1.061	6836
4	28.78	251.90	793.2	1.017	1.313	1.074	10397
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio TSTM Mcf/bbl.
1	0.97	534	1.53	.910	A.P.I. Gravity of Liquid Hydrocarbons
2	1.02	515	1.47	.892	Specific Gravity Separator Gas .580 X X X X X X X X
3	1.07	514	1.47	.888	Specific Gravity Flowing Fluid X X X X X
4	1.18	503	1.44	.867	Critical Pressure 672 P.S.I.A. P.S.I.A.
5.					Critical Temperature 350 °R °R

NO.	P _t ²	P _w ²	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 5.139$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.197$
1	3432.0	11779	389		AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 33,239$	
2	3377.0	11404	764			
3	3269.6	10821	1347			
4	3130.5	9800	2368			
5						

Absolute Open Flow 33,239 Mcfd @ 15.025		Angle of Slope θ	Slope, n 0.71
Remarks:			
Approved By Commission:	Conducted By: H. L. Smith	Calculated By: Wonna Hollis	Checked By: