

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS

Form C-122
Revised 9-1-65

RECEIVED
FEB 22 1972

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 2-7-72	
Company Pennzoil United, Inc.			Connection None		B. C. C. ARTESIA, OFFICE
Pool South Carlsbad (Morrow)			Formation Morrow		
Completion Date 2-4-72		Total Depth 11,833		Plug Back TD 11,762	Elevation 3232 KB
Farm or Lease Name Gulf-Federal					
Csg. Size 5 1/2	Wt. 17# 20#	d 4.892 4.778	Set At 11,830	Perforations: From 11,397 To 11,539	
Well No. 2					
Tbg. Size 2 1/16	Wt. 3.25	d 1.750	Set At *10,298	Perforations: From To	
Unit L 6 23 S 27 E					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple				Packer Set At 10,311	
County Eddy					
Producing Thru Tubing		Reservoir Temp. °F 192 @ 11,300		Mean Annual Temp. °F 60	
				Baro. Press. - P _a 13.2	
State New Mexico					
L 11,468	H 11,468	Gg	% CO ₂	% N ₂	% H ₂ S
Prover		Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI						80	3423			
1.	4.0		2.0	400	6	90	2125			1 Hr
2.	4.0		2.0	400	8	96	1700			1 Hr
3.	4.0		2.0	400	9	110	1298			1 Hr
4.	4.0		2.0	400	10	120	1075			1 Hr
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	19.81	49.74	413.2	.9723	1.310	1.029	1293
2	19.81	57.49	413.2	.9671	1.310	1.028	1483
3	19.81	60.98	413.2	.9551	1.310	1.025	1549
4	19.81	64.28	413.2	.9469	1.310	1.023	1616
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.	.62	550	1.55	.944	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	.62	556	1.57	.947	Specific Gravity Separator Gas .583
3.	.62	570	1.61	.952	Specific Gravity Flowing Fluid XXXXX
4.	.62	580	1.64	.955	Critical Pressure 672 P.S.I.A.
5.					Critical Temperature 354 °R

P _c 3441.2	P _c ² 11841	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.1438$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.0920$
NO.	P _t ²	P _w	P _w ²
1		2194.2	4815
2		1817.2	3302
3		1422.2	2023
4		1220.2	1489
5			

Absolute Open Flow 1765 Mcfd @ 15.025		Angle of Slope 56° 46'	Slope, n .655
Remarks: 2 3/8" EUE N-80 1.995 ID 4.7# Tubing 10,298 to 10,311'			

Approved By Commission:	Conducted By: J. N. Casparis	Calculated By: H. L. Hagler	Checked By:
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WEST TEXAS ENGINEERING SERVICE, INC.