

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

C-12-2
Revised 9-1-65

RECEIVED

Type Test ☐ Initial ☒ Annual ☐ Special						Test Date 8-4-73		AUG 21 1973	
Company Midwest Oil Corp.,				Connection El Paso					
Pool So. Carlsbad				Formation Morrow				Unit O. C. C. ARTESIA, OFFICE	
Completion Date 11-1-73		Total Depth 11850		Plug Back TD 11,759		Elevation GL 3299 KB 3317.5		Farm or Lease Name State "W"	
Csq. Size 4 1/2	Wt. 11.60	d 3.995	Set At	Perforations: From 11331 To 11665		Well No.			
Thq. Size 2 3/8	Wt. 4.7	d 1.98	Set At 11,212	Perforations: From To		Unit G 3 23 26			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Dual						Packer Set At 11,206		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 200 @ 11,493		Mean Annual Temp. °F 70		Baro. Press. - P _a 13.2		State New Mexico	
L 11,493	H 11,493	G _g .586	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run Orice	Taps Flg.	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI							2960	60		
1.	4.026		1.5	7.3	2.6	76	1770	64	Dual	Comp.
2.	"		"	7.3	3.0	76	1372	68		
3.	"		"	7.3	3.4	78	1050	70		
4.	"		"	7.3	3.8	80	660	74		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	10.84	L-10		.9850	1.306	1.039	869.5
2.	"			.9850	"	1.039	1003.3
3.	"	(3.162)		.9831	"	1.039	1134.9
4.	"			.9813	"	1.036	1262.4
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio _____ Dry _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

P _c *2983.4 P _c ² 8901				
NO.	P _c ²	P _w	P _w ²	P _c ² - P _w ²
1	*	2062.5	4254	4647
2	*	1517.2	2302	6599
3	*	1368.9	1874	7027
4	*	1116.0	1245	7656
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$ _____

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____

(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$ _____

1468

Absolute Open Flow _____ 1468 _____ Mcfd @ 15.025	Angle of Slope @ _____ 45 _____	Slope, n _____ 1.000 _____
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Remarks: * P_c & P_w calculations from known bottom hole pressures that were taken during the test.

Approved By Commission:	Conducted By: C. A. Dorsey	Calculated By: M. L. Leierer	Checked By: C. A. Dorsey
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