NE EXICO OIL CONSERVATION COMMISSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED
JUL 16 1973
O. C. C.
ARTESIA, OFFICE

Type Test: [X] Initial [ ] Annual [ ] Special				Test Date: 7-9-73	
Company: J. M. Huber Corp.		Connection: Transwestern			
Pool: South Carlsbad		Formation: Morrow		Unit	
Completion Date: 2-21-73	Total Depth: 11,951	Plug Back TD: 11,669	Elevation: GL 3279	Farm or Lease Name: Terra State	
Csg. Size: 7 5/8 / 4 1/2	Wt.: 26.4 / 11.6	d: 6.969 / 4.000	Set At: 9723 / 11,932	Perforations: From 11,381 To 11,650	Well No.: 1
Tbg. Size: 2 1/2	Wt.: 6.5	d: 2.441	Set At: 11,359	Perforations: From To	Unit: — Sec.: 14 Twp.: 23S Rge.: 26E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single			Packer Set At: 11,359		County: Eddy
Producing Thru: Tbg.	Reservoir Temp. °F: 197 @ 11,359	Mean Annual Temp. °F: 60	Baro. Press. – P_a: 13.2		State: New Mexico
L: 11,359	H: 11 359	Gg: 0.576	% CO_2:	% N_2:	% H_2S: Prover: Meter Run: 4 Taps: Flange

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							3359.0				72
1.	4	X	2.250	631.0	27.0	53	2840.0				24
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	25.64	131.9	644.2	1.007	1.318	1.054	4731
2.							
3.							
4.							
5.							

NO.	P_t	Temp. °R	T_t	Z
1	0.96	513	1.48	0.901
2.				
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
Specific Gravity Separator Gas 0.576 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure 672 P.S.I.A. _____ P.S.I.A.
Critical Temperature 346 R _____ R

P_c 3372.2 P_c^2 11371.7

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		2899.2	8405.4	2966.3
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.834$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 2.660$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 12.584$

Absolute Open Flow 12.584 Mcfd @ 15.025 Angle of Slope θ 54 Slope, n 0.728

Remarks: Produced 7 bbls. liquid

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Paul E. Powers	Paul E. Powers	D. D. Holcomb