

NEW MEXICO CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 3-20-73		MAR 26 1973	
Company Skelly Oil Company				Connection El Paso				O. C. C.	
Pool Cedar Canyon - Morrow				Formation Morrow				Unit ARTESIA, OFFICE	
Completion Date 3-6-73		Total Depth 13,859		Plug Back TD 13,728		Elevation 2979 GR		Farm or Lease Name Cedar Canyon 10 Com	
Csg. Size 5"	Wt. 17.93	d 4.892	Set At 13,859	Perforations: From 13,074 To 13,366				Well No. 1	
Tbg. Size 2-7/8	Wt. 6.5	d 2.441	Set At 12,896	Perforations: From To				Unit Sec. Twp. Rge. F 10 24S 29E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single - Gas						Packer Set At 12,856		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 194°@ 13,380		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State New Mexico	
L 13,220	H 13,220	G _g .581	% CO ₂ .90	% N ₂ .92	% H ₂ S --	Prover --	Meter Run 4	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							4390	72	Packer		
1.	4		2.500	670	30.0	64	2126	80			2 hrs.
2.	4		2.500	665	26.3	58	2340	67			2 hrs.
3.	4		2.500	660	21.5	60	2632	66			2 hrs.
4.	4		2.500	660	17.0	60	2900	65			2 hrs.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	32.64	143.164	683.2	.9962	1.312	1.053	6431
2	32.64	133.554	678.2	1.002	1.312	1.054	6040
3	32.64	120.307	673.2	1.000	1.312	1.054	5430
4	32.64	106.979	673.2	1.000	1.312	1.054	4829
5.							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	3.35	540	1.56	.8002	--	--	.581	X X X X X X X X	675	346
2	3.63	527	1.52	.7800				X X X X X		
3	4.02	526	1.52	.7844						
4	4.39	525	1.52	.7948						
5.										

P _c 4403.2 P _c ² 19,388.2				$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.35732$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.3474$	
NO	P _t ²	P _w	P _w ²	P _c ² - P _w ²			
1		2259.2	5104.0	14284.2			
2		2449.2	5998.6	13389.6			
3		2716.2	7377.7	12010.5			
4		2966.2	8798.3	10589.9			
5							

Absolute Open Flow 8665 Mcfd @ 15.025				Angle of Slope ϕ 976	
Remarks:					
Approved By Commission:					
Conducted By: Joe Banks		Calculated By: Jimmy D. Yancy		Checked By:	