

N MEXICO OIL CONSERVATION COM. 'ON
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-63

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 1-31-73		FEB 8 1973	
Company Texas International Petroleum Corporation				Connection shut in pending connection			O. C. C. ARTESIA, OFFICE	
Pool South Carlsbad (Atoka)				Formation Atoka			Unit	
Completion Date 1-20-73		Total Depth 12000		Plug Back TD 11902		Elevation 3203.8' DF		Farm or Lease Name Tidwell "A" COM
Csg. Size 5	Wt. 17# 20#	d 3.434	Set At 11984	Perforations: From 10754 To 10760		Well No. 1		
Tbg. Size 2-7/8	Wt. 6.5	d 11300	Set At	Perforations: From To		Unit Sec. Twp. Rge. E 8 235 27E		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Multiple (G.G.)					Packer Set At 11300		County Eddy	
Producing Thru Annulus		Reservoir Temp. °F 181 @ 11976		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico
L 10754	H 10754	Gg .604	% CO ₂ -	% N ₂ -	% H ₂ S -	Prover -	Meter Run 3	Taps Flange

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3886	-	5436	38	38
1.	3.068	x	1.50	500	13	68	Morrow	zone	4032	54	1
2.	3.068	x	1.50	500	33	61	COMPLETED		3165	58	1
3.	3.068	x	1.50	690	39	80	IN TUBING		2371	67	1
4.	3.068	x	1.50	690	40	71			1630	64	1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	11.13	81.68	513.2	.9924	1.287	1.043	1211
2	11.13	130.14	513.2	.9990	1.287	1.045	1931
3	11.13	165.60	703.2	.9813	1.287	1.056	2458
4	11.13	167.71	703.2	.9896	1.287	1.059	2518
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.76	528	1.47	.919	169	56	.604	X X X X X	671	360
2.	.76	521	1.45	.915				X X X X X	671	366
3.	1.05	540	1.50	.897						
4.	1.05	531	1.48	.892						
5.										

P _c 5449.2 P _c ² 29,694				$(1) \frac{P_c^2}{P_c^2 - P_w^2} = \frac{29,694}{26,992}$		$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.100$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2,770$		
1	16,364	4045.5	16,366	13,328			
2	10,101	3179.3	10,108	19,586			
3	5,684	2386.4	5,695	23,999			
4	2,700	1643.7	2,702	26,992			
5							

Absolute Open Flow 2,770 Mcfd @ 15.025		Angle of Slope @ 45°	Slope, n 1
Remarks: Calculations made by electronic calculator			
Approved By Commission:	Conducted By:	Calculated By: D.E. Simpson	Checked By: