

W MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS

Form C-122
Revised 9-1-65

RECEIVED

FEB 8 1973

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 1-31-73			
Company Texas International Pet. Corp.				Connection Shut in pending connection.			O. C. C. ARTESIA, OFFICE	
Pool South Carlsbad (Morrow) Gas				Formation Morrow			Unit ---	
Completion Date 1-24-73		Total Depth 12,000		Plug Back TD 11,902		Elevation 3203.8' DF		Farm or Lease Name Tidwell "A" COM
Csg. Size 5-1/2"	Wt. 17#, 20#	d 4,778	Set At 11,984	Perforations: From 11,426 To 11,824		Well No. 1		
Tbg. Size 2-7/8"	Wt. 6.5#	d 2,441	Set At 11,300	Perforations: From --- To ---		Unit E	Sec. 8	Twp. Rye. 23-S 27-E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Multiple (G.G.)					Packer Set At 11,300		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 181 @ 11,976		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico
L 11,300	H 11,300	Gg .589	% CO ₂ ---	% N ₂ ---	% H ₂ S ---	Prover ---	Meter Run 3	Taps Flange

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3886	66	5436	---	46
1.	3.068 x 2.00			685	8	74	3367	64	Atoka zone		1
2.	3.068 x 2.00			685	18	66	3006	65	Completed in		1
3.	3.068 x 2.00			700	27	66	2650	60	annulus.		1
4.	3.068 x 2.00			765	37	68	2193	62			1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	21.32	74.74	698.2	.9868	1.303	1.054	2160
2	21.32	112.11	698.2	.9943	1.303	1.056	3270
3	21.32	138.77	713.2	.9943	1.303	1.058	4055
4	21.32	169.69	778.2	.9924	1.303	1.063	4973
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	1.04	534	1.51	.900	226	60	.589	X X X X X X X X	672	354
2.	1.04	526	1.49	.896			X X X X X			
3.	1.06	526	1.49	.894						
4.	1.16	528	1.49	.885						
5.										

P _c 3899.2 P _c ² 15,204					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{15,204}{10,082}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.355$	
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²				
1	11,426	3388.0	11,479	3,725				
2	9,116	3038.6	9,233	5,971				
3	7,093	2,695.5	7,266	7,938				
4	4,867	2,263.2	5,122	10,082				
5								

Absolute Open Flow 6,738 Mcfd @ 15.025					Angle of Slope θ 53.5		Slope, n .740		
Remarks: Calculations made by electronic calculator.									
Approved By Commission:			Conducted By:			Calculated By:		Checked By:	
						D. E. Simpson			

Sealed 2-12-73