

**NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

RECEIVED

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122*

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 10-2-73		OCT 9 1973		
Company J. M. Huber Corp.				Connection Transwestern Pipeline Co.				O. C. C.	
Pool South Carlsbad				Formation Morrow				Unit ARTESIA, OFFICE	
Completion Date 5-3-73		Total Depth 11,960		Plug Back TD 11,900		Elevation 3313 GL		Farm or Lease Name Yates King	
Csg. Size 4 1/2"	Wt. 11.6	d 4.000	Set At 11,960	Perforations: From 11,633 To 11,688			Well No. 1		
Tbg. Size 2 1/2"	Wt. 6.4	d 2.441	Set At 11,618	Perforations: From open end To 			Unit Sec. Twp. Rge. K 22 23S 26E		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 11,618		County Eddy		
Producing Thru Tbg.		Reservoir Temp. °F 193, 11,515'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2		State New Mexico	
L 11,618	H 11,618	Gg 0.591	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run 4"	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1349.0		Packer		95
1.	4 X 0.750			660.0	24.0	90	709.0				24
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	2.661	127.1	673.2	0.9723	1.301	1.037	444
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bol.
1.	1.00	550	1.64	0.930	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas 0.591 XXXXXXXXXX
3.					Specific Gravity Flowing Fluid XXXXXX
4.					Critical Pressure 673 P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature 336 R _____ R

* P_c **1751.2** P_c^2 **3066.7**

NO	F _t	P _w	P _w ²	P _c ² - P _w ²
1	*	1479.2	2188.0	878.7
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \underline{\underline{3.490}}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{\underline{2.481}}$

ADP = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{\underline{1.102}}$

Absolute Open Flow 1.102 Mcfd @ 15.025	Angle of Slope θ 54	Slope, n 0.727
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Remarks: * P_f & P_s measured by A & A Engineering Company of Midland Texas

Approved By Commission:	Conducted By: L. Goodenough P. Powers	Calculated By: <i>Paul C. Powers</i>	Checked By: <i>W. H. H. H. H.</i>
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