

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

JAN 25 1974

Type Test ☐ Initial ☐ Annual ☒ Special				Test Date 1/8/74		JAN 25 1974	
Company Exxon Company, U.S.A.				Connection El Paso Natural Gas		O. C. C. ARTESIA, OFFICE	
Pool South Carlsbad				Formation Morrow Gas		Unit --	
Completion Date 6/18/73		Total Depth 11,991'		Plug Back TD 11,847'		Elevation 3,285 KB	
Farm or Lease Name So. Carlsbad Gas Com. No. 2				Well No. 1			
Csg. Size 3 1/2"	Wt. 9.2 lb.	d 2.992	Set At 11,990'	Perforations: From 11,433' To 11,797'		Unit Sec. Twp. Rge. N 23 235 26F	
Tbg. Size --	Wt. --	d --	Set At --	Perforations: From w/65 holes To			
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single, Tubingless Completion				Packer Set At None		County Eddy	
Producing Thru Casing		Reservoir Temp. °F 202 @ 11,615'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2	
State New Mexico							
L 11,615'	H --	Gg .58	% CO ₂ 1.4	% N ₂ 0.15	% H ₂ S 0.00	Prover --	Meter Run F

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	3238 BHP										24 hrs.
1.	4	X	2.75	365	4.6	68	2481				4 "
2.	4	X	2.75	365	10.2	64	2233				4 "
3.	4	X	2.75	378	26.0	60	1956				4 "
4.	4	X	2.75	396	62.4	66	1262				4 "
5.	4	X	2.75	403	73.1	66	947				4 "

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	46.54	42	378	.9924	1.311	1.029	2617
2.	46.54	62.2	378	.9962	1.311	1.030	3894
3.	46.54	101	391	1.000	1.311	1.032	6359
4.	46.54	159	410	.9943	1.311	1.033	9964
5.	46.54	174	416	.9943	1.311	1.033	10,904

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	.56	528	1.55	.950	Dry Gas	--	.58	X X X X X X X X	679	340
2.	.56	524	1.54	.950						
3.	.58	520	1.53	.949						
4.	.60	526	1.55	.948						
5.	.61	526	1.55	.9475						

NO.	P _t ²	P _w	P _w ²	P _t ² - P _w ²
1.	--	3054	9326.9	1,159.7
2.	--	2943	8661.2	1,825.3
3.	--	2624	6885.4	3,601.2
4.	--	1865	3478.2	7,008.4
5.	--	1574	2477.5	8,009.1

(1) $\frac{P_c^2}{P_t^2 - P_w^2} = 1.309$

AOF = Q $\left[\frac{P_c^2}{P_t^2 - P_w^2} \right]^n = 13,263$

(2) $\left[\frac{P_c^2}{P_t^2 - P_w^2} \right]^n = 1.216$

Absolute Open Flow	13,263	Mcfd @ 15.025	Angle of Slope @	54°	Slope, n	.727
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Remarks: Flowing pressures used for calculations were measured with a bomb @ 11,800'.

Approved By Commission:	Conducted By: Exxon Company, U.S.A.	Calculated By: S.E. Palko <i>Sp</i>	Checked By: A.M. Jack <i>Am</i>
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