

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 1-15-74		JAN 29 1974		
Company J. M. Huber Corporation				Connection Transwestern Pipeline Co.				O. C. C. ARTESIA, OFFICE	
Pool South Carlsbad				Formation Morrow				Unit	
Completion Date 7-10-73		Total Depth 11,922		Plug Back TD 11,876		Elevation KB 3255		Farm or Lease Name Moore "Com"	
Csg. Size 4 1/2"	Wt. 11.6	d 4.000	Set At 11,892	Perforations: From 11,515 To 11,618		Well No. 1			
Teg. Size 2 7/8"	Wt. 6.4	d 2.441	Set At 11,482	Perforations: From To		Unit 35		Sec. Twp. Rge. 23S 26E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single					Packer Set At 11,482		County Eddy		
Producing Thru Tbg.		Reservoir Temp. °F 199 @ 11,565		Mean Annual Temp. °F		Baro. Press. - P _a 13.2		State New Mexico	
L 11,567	H 11,567	Gg 0.578	% CO ₂	% N ₂	% H ₂ S	Prover	Meter Run 4"	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							2141.0				72
1.	4 X 1,250"			560.0	16.0	58	1156.0				24
2.											
3.											
4.											
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	7,520	95.77	573.2	1.002	1.315	1.045	992
2.							
3.							
4.							
5.							

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1.					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.					Specific Gravity Separator Gas _____ X X X X X X X X
3.					Specific Gravity Flowing Fluid _____ X X X X X
4.					Critical Pressure _____ P.S.I.A. _____ P.S.I.A.
5.					Critical Temperature _____ R _____ R

* $P_c = 2770.2$ $P_c^2 = 7674.0$

NO.	P_t^2	P_w	R_w^2	$P_c^2 - R_w^2$
1	*	1766.2	3119.5	4554.5
2				
3				
4				
5				

(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.685$ (2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.413$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1,402$

Absolute Open Flow <u>1,402</u> Mcfd @ 15.025		Angle of Slope θ <u>56.5</u>	Slope, n <u>0.663</u>
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Remarks: * P_f and P_s measured by Bennett Wire Line Service Artesia, New Mexico

Approved By Commission:	Conducted By: L. Goodenough P. Powers	Calculated By: <i>Paul Powers</i>	Checked By:
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