

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

well file
Form O-122
Revised 9-1-65
RECEIVED

NOV - 11

Type Test		☒ Initial		☐ Annual		☐ Special		Test Date		10-30-73	
Company				Location				O.F.C.			
MOORE OIL CORP.				—				ARTESIAN			
Pool				Formation				Unit			
SOUTH CAROLAS BADMERON				MOORE				300			
Completion Date		Total Depth		Blow By At		Elevation		Form or Log No.			
10-12-73		12050		11922		3244 G.L.		FED. MIN. Comm			
Casing Size	Wt.	Set At	Perforation	From	To	Well No.					
7"	26 1/4	6.216	12048	11658	11878	#1					
Tub. Size	Wt.	Set At	Perforation	From	To	Unit		Sec.		Twp. Rge.	
2 3/8"	4.6 1/2	1.995	11651			F		13		235 24-E	
Type Well - Single - Brokenshot - G.G. or G.O. Multiple						Sec. At		County			
SINGLE						11634		EDDY			
Producing Thru		Reservoir Temp. °F		Mean Annual Temp. °F		Daily Flow - B ₂		State			
TUBING		180-12050		60°		13.2		NEW MEXICO			
L	H	G _g	% CO ₂	SH ₂	SH ₂ S	Prover	Meter Run	Days			
11651	11768	0.5854	1.14	0.33	—	—	4"	FLANGE			

FLOW DATA							TUBING DATA		CASING DATA		Duration
NO	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	of Flow
SI	4" X 1.5"						3015	70	—0—	—	7252.5 L
1.	4 X 1.5"			605	15	78	2730	70	—0—	—	142
2.	4 X 1.5"			605	26	69	2400	70	—0—	—	142
3.	4 X 1.5"			605	40	64	2085	70	—0—	—	142
4.	4 X 1.5"			605	61	57	1570	70	—0—	—	142
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor F _{sp}	Rate of Flow Q, Mcfd
1	10.84	96.3	618.2	1.9831	1.307	1.045	1412
2	10.84	126.8	618.2	1.9915	1.307	1.047	1865
3	10.84	152.2	618.2	1.9962	1.307	1.052	2330
4	10.84	174.2	618.2	1.003	1.307	1.054	2909
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
					∞	
1	.91	538	1.53	1.916	A.P.I. Gravity of Liquid Hydrocarbons	—
2	.91	529	1.51	1.912	Specific Gravity Separator Gas	XXXXXX
3	.91	524	1.49	1.903	Specific Gravity Filling Fluid	XXXXX
4	.91	517	1.47	1.900	Critical Pressure	676 P.S.I.A.
5					Critical Temperature	351 R

NO.	P _r	P _w	P _r ²	P _w ²	P _r ² - P _w ²	(1) $\frac{P_r^2}{P_r^2 - P_w^2}$	(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n$
1	7525	2155	7592	1578			
2	5824	3434	3944	3224			
3	4402	2145	4595	4575			
4	2507	1678	2925	1355			
5							

$P_c = 2528.2$ $P_c^2 = 9169.99$
 (1) $\frac{P_r^2}{P_r^2 - P_w^2} = 1.443$ (2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 1.2725$
 ACFT = 2 $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 3702$

Absolute Oper. Flow 3702 Mcfd @ 15.025 Angle of Slope 56° 45' Slope, n 1.65526

Remarks: _____

Approved By Commission: _____ Conductor By: T.O. NEWTON Calculated By: A.R. BLANEDDINE Checked By: A.R. BLANEDDINE