

W MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Copy 651
Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-3-73		NOV 29 1973	
Company C & K PETROLEUM, INC.				Connection NOT CONNECTED		O. C. C.	
Pool WILDCAT				Formation CLISCO - CANYON		Unit ARTESIA, OFFICE	
Completion Date 10-3-73		Total Depth 10,250'		Plug Back TD 8673'		Elevation 4050 DF	
Farm or Lease Name LOWE - STATE		Well No. 1		Perforations: From 8376' To 8406'		Unit Sec. Twp. Rge. C 16 24S 24E	
Csg. Size 5 1/2" O.D.		Wt. 17#		Set At 8640'		Perforations: OPEN ENDED To	
Tbg. Size 2" EUE		Wt. 4.70#		Set At 8241'		County EDDY	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 8241'		State NEW MEXICO	
Producing Thru TUBING		Reservoir Temp. °F 162@ 8325		Mean Annual Temp. °F		Baro. Press. - P _a 13.2	
L 8241'		H 8241'		Gg .608		% CO ₂ .55	
				% N ₂ .15		% H ₂ S -	
Prover		Meter Run 4.000		Taps FLANGE			

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI	90 HRS.					2687		PACKER		
1.	4.000 x	1.75"	403	24"	92	2645		"		60 MIN.
2.	DITTO		452	50"	71	2601		"		60 "
3.	"		807	57	64	2516		"		60 "
4.	"		917	91	56	2378		"		60 "
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	14.93	99.940	416.2	.9706	1.282	1.030	1912
2	14.93	152.514	465.2	.9896	1.282	1.038	2999
3	14.93	216.222	820.2	.9962	1.282	1.072	4420
4	14.93	290.940	930.2	1.0040	1.282	1.091	6100
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1	.62	552	1.54	.943	A.P.I. Gravity of Liquid Hydrocarbons <u>NOT AVAILABLE</u> Deg.
2	.69	531	1.48	.928	Specific Gravity Separator Gas <u>0.608</u> X X X X X X X X
3	1.22	524	1.46	.870	Specific Gravity Flowing Fluid <u>X X X X X</u>
4	1.38	516	1.44	.840	Critical Pressure <u>674</u> P.S.I.A. _____ P.S.I.A.
5					Critical Temperature <u>358</u> R _____ R

P _c 3301.2 P _c ² 10898				
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²
1		3271.2	10701	197
2		3245.2	10531	367
3		3213.2	10325	573
4		3173.2	10069	829
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 13.146$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 46,824$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 7.676$$

Absolute Open Flow <u>46,824</u> Mcfd @ 15.025	Angle of Slope θ <u>51.5°</u>	Slope, n <u>.796</u>
Remarks: _____		
Approved By Commission: _____ Conducted By: <u>Nancy E. Segura</u> Calculated By: _____ Checked By: _____		