

N MEXICO OIL CONSERVATION COM SION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

RECEIVED

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 8-25-78		AUG 29 1978 O. G. C. ARTESIA, OFFICE	
Company C & K Petroleum Inc. ✓				Connection El Paso Natural Gas			
Well Crooked Creek <i>Morrow</i>				Formation Morrow			
Completion Date 8-6-78		Total Depth 10,250'		Plug Back TD 10,116		Elevation 4050 Gr.	
Csg. Size 4" Liner		Set At 8271		Perforations: From 9721 To 10,021		Well No. 1	
Trq. Size 2-3/8		Set At 8271		Perforations: From open To end		Unit Sec. Twp. Rge. C 16 24-S 24-E	
Type Well - Single - Prodenhead - G.C. or G.O. Multiple Single				Packoff Set At 8271'		County Eddy	
Producing Thru Tubing		Reservoir Temp. °F 145 @ 9871		Mean Annual Temp. °F 132		Baro. Press. - P _a 13.2	
L H Gg		% CO ₂ Nil		% N ₂ Nil		% H ₂ S Nil	
		Prover		Meter Run 4.026		Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1	4.026		.750	7.8	4.0	95	2200				
2	"		"	7.8	5.7	90	1222	80			60
3	"		"	7.9	7.4	95	1150	82			60
4	"		"	8.0	9.0	95	1015	84			60
5						95	800	86			60

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow O, M/d
1				.9680	1.222	1.054	327
2	2.661			.9723	"	1.058	468
3	1-10			.9680	"	1.056	648
4	100" x 1000 psi			.9680	"	1.058	758

NO.	P _i	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1					None					
2										
3										
4										
5										

$P_c = 2850.4$ $P_c^2 = 8125$ $B.H.P.$				
NO.	P_i^2	$P_w^2 P_f$	$P_w^2 P_f^2$	$P_c^2 - P_i^2$
1		2788.9	7778	347
2		2733.7	7473	652
3		2641.4	6977	1148
4		2494.4	6222	1903

$$(1) \frac{P_c^2}{P_c^2 - P_i^2} = 7.077$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_i^2} \right]^n = 2030$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_i^2} \right]^n = 3/133$$

Absolute Open Flow	2030	Md/d @ 15.025	Angle of Slope @	59.5	Slope, n	5836
Remarks:						

Approved By Consultant:	Conducted By:	Calculated By:	Checked By:
	C. Allen Dorsey	C. Allen Dorsey	